Rocky Flats Environmental Technology Sites Actinide Migration Evaluation

Meetings January 8-9, 2001
Advisory Group
Greg Choppin, David Clark, David Janecky, Leonard Lane,
A J Francis and Anne Kersting

Summary and recommendations for path forward

The Pathway Report is making progress (overview, air, chemistry/geochemistry, biological, groundwater) An important component will be the strong technical basis with clear separation of basic information from model description and applications to specific RFETS areas and problems. The document is building upon the solid basis of the Conceptual Model Report, with careful definition of the technical aspects of actinide chemistry, treatment of misguided simplification approaches to some of the problems (e.g. KD usage for Plutonium^(Pu) and Americium^(Am) groundwater migration evaluation) and collection of documentation of RFETS monitoring. It is critical that this document be the technical basis for Sampling and Analysis Plans for RFETS Industrial Area, Protected Area, Process Waste Line, and buffer zone—integrated characterization, D&D remedial actions, and long-term stewardship

Stewardship needs to be more carefully promulgated through the chain of work at RFETS (ER, D&D, and communications)

Uranium^(U) sources and old borings data found by Laurie Gregory-Frost and Bob Smith is great. We really appreciate the diligence of the RFETS personnel that work on AME projects, especially such efforts to find and integrate historical data to provide a fully textured view for AME.

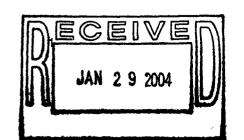
Progress and integration

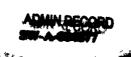
Land configuration is an area that we are pleased to see being considered in the context of the Pathway Analysis and in relationship to the erosion and water balance modeling efforts. It is good to see a contract in place for integrated emphasis at the Sites. Participation by the RFETS contractors in this AME meeting was an important initial step in making sure that actinide migration evaluation issues are fully coupled. We are very interested in hearing about their plans, procedures and progress during future AME advisory meetings.

We feel that Sites Management is positive and proactive in its approach to stewardship and stakeholder participation. The AME advisors view this as a critical component of successful closure of the RFETS Sites.

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Results and Discussions

Updates on the Water Balance Modeling – Dayton

As part of developing a detailed design basis for closure activities RFETS is conducting a Sites-wide Water Balance (SWWB) Project—The SWWB will develop a management tool in the form of a physically-based, integrated model This model may be applied to various RFETS Closure decisions

Following development of the conceptual hydrologic model for RFETS, a draft, comparative study was completed to select an appropriate model code. The MIKE SHE software was selected as the best system to meet the project objectives.

Most of the Sites environmental data collected during the calibration period has been compiled. Data analysis at this stage of model calibration consists of preparation of data inputs (i.e. model drivers) and calibration targets. Listed below are the status of the wind, surface water and groundwater data inputs.

- Wind data from the perimeter wind and air quality monitoring stations maintained by CDPHE were analyzed
- All surface water data have been compiled, and responses for the entire year at all gauging stations have been plotted against event duration and magnitude
- All quarterly groundwater level data up to and including 10/00 have been collected, and Hermit continuous water level data have been retrieved, but not been checked for accuracy and completeness

Update on the Erosion and Sediment Transport Modeling –Wetherbee

There was a discussion of representation of rip/rap drop structures in the sediment transport model, HEC-6T. Previous modeling efforts used two models and averaged the results. Subsequent review comments suggested this was arbitrary. The most recent modeling represented the rip/rap structures as a serrated configuration with and without channel erosion. Computed sediment yields are now between those of the original drop structure modeling results and those from modeling the channels without drop structures. The flow velocities now look reasonable, and they are examining the maximum velocities for the 100 yr event, Some of the velocities are on the order of some 20 ft/sec.

The relative proportions of channel and hillslope sediment yields are now being studied. Channel erosion is now integrated into all sediment yield models. Some interesting features have been found that were not included in previous models (e.g. stock pond in Noname gulch).

Efforts are underway to evaluate taking out some ponds at closure Changes in simulated sediment yield with and without Pond C-1 are being investigated. Simulated sediment yields increased and additional analyses are needed for actinide transport evaluation. Removing all but terminal ponds in Walnut Creek resulted in a 30% increase in sediment yield. Removing all but

Pond B-5 resulted in a 50% to 90% increase in sediment yield. With no detention ponds, sediment yields were estimated to increase by about 60-94%.

Wright Water Engineers personnel summarized future efforts as follows Greg Weatherbee will program some future scenarios and continue modeling channel processes, Ian Paton will model actinide transport, Chris Hawley will conduct additional erosion simulation, and Margaret Herzog will be writing programs to automate linking the erosion, sediment transport, and actinide transport calculations

Leonard Lane suggested that they develop data management routines to track changes in erosion modeling through the sediment transport calculations and then through the actinide transport calculations. Greg Wetherbee responded that they are working to accomplish this automated linking but have not completed it and referred to the work by Margaret Herzog. Greg Wetherbee also stated that they are working to link QA/QC to the data management programs and will get together with personnel conducting the land use/configuration work next week.

In a follow up, Dave Clark suggested they carefully examine reversals in sediment yields with changing assumptions to see if they are reasonable and consistent across all watersheds. Leonard Lane suggested comparing their reservoir sediment routing results with some standard reservoir trap efficiencies as a generalized test of the sediment transport modeling.

Wright Water Engineers personnel stated that they hope to have the sediment transport modeling and revisions in place within the next 4-6 weeks and then move forward to the actinide evaluations

Overview of the Pathway Analysis Report -- Paton

A general overview was presented on the general outline for the pathway report. The general approach to the pathway report is to follow the general outline of the conceptual model document that has been used effectively as a tool for public communication and involvement. The amount of material is so large, that it was wisely decided to break the report down into two documents. The primary document will be a summary report outlining the general philosophy, conceptual model, and scientific understanding of actinide chemistry, geochemistry, and transport that affect actinide migration at RFETS. The secondary document will be a sizeable technical appendix that covers the following 1) background, 2) actinide geochemistry, 3) RFETS actinide data, 4) pathway analysis based on measured data, 5) pathway analysis based on modeled data, 6) a comparison of measured/modeled data, 7) links to comprehensive risk assessment, and 8) overall summary and comparison of major pathways

We strongly agree with this two-report philosophy. We also suggest that the primary document should remain relatively short (50-100 pages) and should be produced with the assistance of a professional editor, and make good use of color graphics. This should be viewed as a high-profile glossy marketing

3

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document for use in marketing the underlying scientific understanding of actinide migration on which future decisions will be based. An example of what we have in mind can be found in the recent volume of Los Alamos Science, 26, 2000 "Challenges in Plutonium Science". We realize that this represents a sizeable effort and cost, but also suggest that such a document will be more readable and useable by the general public, stakeholders, regulators, and political representatives

The technical appendix can and should contain the bulk of the technical information, and is expected to get quite large. We also suggest that appendix section 3, "Measured RFETS Actinide Data" be moved forward to follow the introduction and background (section 1). In this way, the major discussion of actinide geochemistry can follow the discussion of measured data, and our understanding of actinide geochemistry can refer to the measured data.

Actinide Pathway Sources and Surface Water Pathway (status and path forward) – Paton & WWE staff

A major focus of discussion by Ian Paton in his presentation was the need for a more quantitative aspect in the Pathway Report, especially in the surface water transport analysis. This had been the major concern of Tom Hakonson in his comments (10/17/99). The original intent was to develop a qualitative analysis as a guide to further AME activities R&D. However, appropriate quantitative data with references are needed to provide a convincing basis for choice of major versus minor pathways and the relative importance of the subpathways within these two classifications (major versus minor). Such a quantitative analysis would be important in choice of topics and the relative emphasis on these in the final report. However, to develop a useful quantitative analysis requires more data on actinide behavior in neutral and basic solutions in different environmental media. This includes good knowledge of the nature of the actinide species present and the thermodynamic and kinetic parameters of the sorption to particulates and surfaces, colloidal formation, migration (dissolved and colloidal), etc.

It seems that more emphasis should be devoted to defining the different behavior patterns of U, Pu, and Am. U is likely to be in the VI oxidation state which would be associated with a significant solubility as simple, molecular sized species (e.g., $UO_2(OH)^+$, $UO_2(CO_3)_3^{4-}$), etc. Americium would be present in the trivalent state with a lower molecular species solubility than U as hydrolysis is the major speciation pathway unless fluoride concentrations are unusually high Plutonium would be, predominately, in the IV oxidation state. This results in a very strong hydrolysis reaction to form $Pu(OH)_4$ which ages to the even more insoluble PuO_2 in H_2O . There is a small solubility of the PuO_2^+ species but its concentration is controlled by the insolubility of $Pu(OH)_4$ and is limited to ca $10^{-8}M$. Consequently, the majority of Pu transported in surface water is present as intrinsic colloids of PuO_2 in H_2O or as pseudo colloids in which PuO_2 is sorbed to other mineral (e.g. Fe_2O_3) and organic (e.g. humic) colloids

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This difference is very important to recognize if quantitative analysis (i.e., modeling) is to be applied to the Pathway Report. U data can be used with models for soluble species (e.g. RESRAD) but such models are not applicable to analyses of Am or Pu behavior in surface water pathways. Use of such soluble species models for Am(III) and Pu(IV) could be successfully challenges legally as they are scientifically incorrect.

Pathway Analysis Report, Section 2 Geochemistry

The Pathway Report is well done. It discusses most issues well and gives pertinent references. The discussion on the merits and limitations of K_D values usage should be useful to other Sitess in their reports as K_D 's are valuable when used within their limitations. The Resume on pages 2.2-2.7 is valuable and should be well cited in the future.

There are several minor and one major concern. First the minor ones. On page 2.10, at the bottom, in the discussion of aqueous complexes, hydrolytic species should - must-be included. Presumably, they were omitted because of the assumption that they are insoluble, however, in contact with insoluble $Pu(OH)_4$ are the soluble $Pu(OH)_1^{(4-n)+}$ species where n=1-3. Also, the most soluble species in neutral/basic systems are the PuO_2^+ species such as $PuO_2CI_2^ Am^{3+}$ has much more $Am(OH)^{(3-n)+}$ present and these species usually are quite significant in the net solubility. It is stated that complexation increases the solubility - true but oxidation of Pu from IV to V is much more important than complexation for increasing Pu concentration in neutral/basic waters. On page 2.19, Fig. 2.4-1, why are all the species Pu_1^{4+} (except a little Pu_2^{3+} at low Pu_2^{3+} 1 is very well established that in natural and sea surface waters, $Pu(V)O^+$ is present at many orders of magnitude higher concentrations than any Pu(IV) species Also Pu(III) is present only in very acidic or highly reducing solutions. I suggest getting a more recent diagram than one from 1985

A discussion of K_D values emphasized the importance of recognizing the correct models to use for actinide species K_D values may represent thermodynamic (reversible) binding of ions to anionic Sitess on solids or extractant ligands soluble in organic phase. However, also, they may reflect sorption of insoluble species to solid surfaces, colloidal sorption to surfaces, precipitation of insoluble species, etc., all of which may be irreversible reactions Rarely are measurements done by methods which define the species involved or which measure the kinetics of sorption/desorption involved in the Ko values Without such knowledge, KD values cannot be used in models which require species reversibility. For example, without understanding the kinetics related to the K_D measurements, models using multiplate sorption/desorption for migration are scientifically invalid. Consequently, based on experimental data correlated with speciation calculations using stability constant, solubility products, the redox speciation calculations both for RF natural waters as well as other Sitess (Hanford, INEEL, sea water, fresh water lakes, etc.), U in near surface oxic waters is present at U(VI)O₂²⁺ species. In this oxidation state, U can be present

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in concentrations of 10^{-6} - 10^{-8} M as carbonato and mixed hydroxy/carbonato species. In anoxic waters, it would be present as U(IV) and this state is highly insoluble (# 10^{-12} M). Consequently, in oxic waters, U behavior can be modeled as soluble species and K_D values can be used

By contrast, Am exists as Am(III) in both oxic and anoxic waters. The hydrolysis of Am(III) is very strong so the soluble Am(III) is very low relative to colloidal species. K_D values, relevant to behavior of soluble monocationic Am(III) species are irrelevant for modeling colloidal Am(III) migration.

Plutonium favors Pu(IV) in oxic, natural waters. Like Am(III), the hydrolyzed $Pu(OH)_4$ is extremely insoluble but sorbs to colloidal material. Pu(IV) does have a redox equilibrium with more soluble $Pu(V)O_2^+$ but the latter, in the presence of $Pu(OH)_4$, the concentration of Pu(V) is limited to $\#10^{-8}M$. The concentration of insoluble Pu(IV) species sorbed on and transported by colloids can be $\#10^{-6}$ M. Consequently, modeling of Pu in natural waters must focus on transport of colloidal Pu(IV) and use of K_D values for soluble Pu equilibria behavior is not acceptable scientifically

Pathway Analysis Report, Biological Pathway

Biological pathway report dealing with the uptake by plants and animals needs to be revised and presented in a concise and coherent manner with supporting documentation showing the soil concentration and bioavailability and the role of microorganism in regulating the bioavailability to higher plants. For example, the report should include the concentrations of Pu, Am, and U in the soil, in plants, and animals. This section should high light the mechanisms of uptake of the actinides from RFETS soils by plants based on the studies conducted at the Sites.

The new section on TA - 1 6 3 Microbiology should address the presence, abundance and distribution of microorganisms at RFETS and its potential role in the mobilization or stabilization of U, Pu, and Am Briefly discuss the role of soil and rhizosphere microorganisms in regulating the bioavailability of actinides to higher plants

The section TA - 2 6 Microbiological Transformations of the report should address the key microbial processes which affect the mobility and stability of actinides as well as the long-term-management and stewardship of the Sites. It should discuss the microbially mediated redox reactions and how it affects the dissolution and precipitation of Pu, and U under wet and dry cycles, bioaccumulation and biosorption of actinides resulting in the immobilization or mobilization as biocolloids in porus media, biotransformation of actinide-organic and inorganic complexes and the fate of released actinide

This section of the report should be integrated with the TA-2 Pu, Am, and U Geochemical, Transport Processes section and should take advantage of the background information discussed in the report which are pertinent to microbial transformations of Pu, Am, and U

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Industrial Area Sampling and Analysis Plan status and schedule – Serreze

The sampling plan describes approaches to determination of the contamination of the Industrial Area D&D aspects looks like a good plan, but ER needs to be more strongly integrated. In the ER plan, in particular, background and differentiation of background from contamination is used extensively, however how background will be determined is not defined. For example, it is well documented that natural U is present across the Sites and variable in concentration, so a background cannot be generally defined. The AME Advisory Group needs to continue to be updated on current status, data, interpretations and plans for underbuilding contamination and old process waste lines.

Uranium sources, transport and disposal – Gregory-Frost

The project to examine historical data for insight into the potential U source term associated with old and new Sites Ponds has progressed rapidly This is largely due to the hard work and dedication of Laurie Gregory-Frost Historical U analyses were presented for soil and pore-water samples analyzed in 1993-1994 These analyses were performed following a remedial action at the Sites Ponds to remove the sludge (pondcrete) and liners Some samples were taken from directly under the ponds, while others were from the adjacent hillside In general the U concentrations found in and around the Sites ponds were very low, and in the pCi/g (soil) or pCi/L (water) range None of the soil samples exceeded the Tier I action level, and pore-water samples only exceeded action levels at three sample locations All three of these were located within the Sites pond boundaries Most important is the fact that the soil cores were sampled all the way down to the bedrock layer, and in no case was a large deposit of U observed Soil samples were all within the 1-60 pCi/g range, while pore-water samples were all within the 1-3,700 pCi/L range Recall that the natural background U in Rock Creek is on the order of 1,200 pCi/L This is a very small amount of U

These historical data go a long way toward establishing the magnitude of the U source term under the Sites pond as a result of past Sites activities. It appears that there is in fact, only a small quantity of U present. This is consistent with the geochemical modeling results of Ball (2000) that suggested that groundwater samples near the Sites ponds were all under-saturated with respect to common U solids. Therefore, the observed retardation of U relative to nitrate is more consistent with sorption/desorption processes. This is also consistent with our expectations for U geochemical behavior, namely that it will be relatively soluble and mobile under the soil and groundwater conditions at RFETS. The fact that there is only a small amount of U present beneath the Sites ponds suggests that the reactive barrier presently installed downslope of the Sites ponds should continue to capture and remediate U as an ancillary role to the treatment of nitrate.

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Stewardship - Shelton

We had a very insightful and illuminating discussion with Kaiser-Hill senior management on long-term stewardship. It was useful to understand that management acknowledges that some actinides will remain on the Sites, and that the South Interceptor Ditch and ponds will likely remain at Sites closure. We like this view from the Senior Management of Kaiser-Hill, but are concerned about how to convey this stewardship concept and approach down to workers. For example, how do we keep balance in areas like decisions on Old Process. Waste Lines and under building contamination. The Advisory Group supports use of the long-term Vulnerability Assessment as an integration process. This will enhance perception and accomplishment of early emphasis on stewardship, and alignment with the stakeholders. The Sites believes it is built into documents, but maybe not as explicitly as required and fully integrated to end-state.

The AME Advisory Group will continue to incorporate this perspective into our activities and evaluations to make sure we are also communicating effectively

Documents provided to advisory group

Meijer, A (1990) Yucca Mountain Project Far-Field Sorption Studies and Data Needs

Ian Paton – Pathway report activity viewgraphs

Martha Hyder – air transport pathway viewgraphs

Pathway report section 3 viewgraphs and maps

Comments on section 2 of technical appendix

Comments on Hersman's text by AJ Francis

R Smith viewgraphs on groundwater pathway progress

Draft Industrial Area Characterization Schedule

Laurie Gregory-Frost -- Sites evaporation ponds soil and water sampling viewgraphs

Ableson stewardship viewgraphs

Summary of NRC August 2000 report on stewardship

Documents and information requested for advisory group

Meyers/McKenna presentation and analysis papers on smart sampling, IA white space

Requests for Future Presentations and Information

Land Configuration team – need early plan presentation and updates on progress, constraints and concerns often after that SAP continuation with team, not separate representative each time

Participants in AMS technical meetings

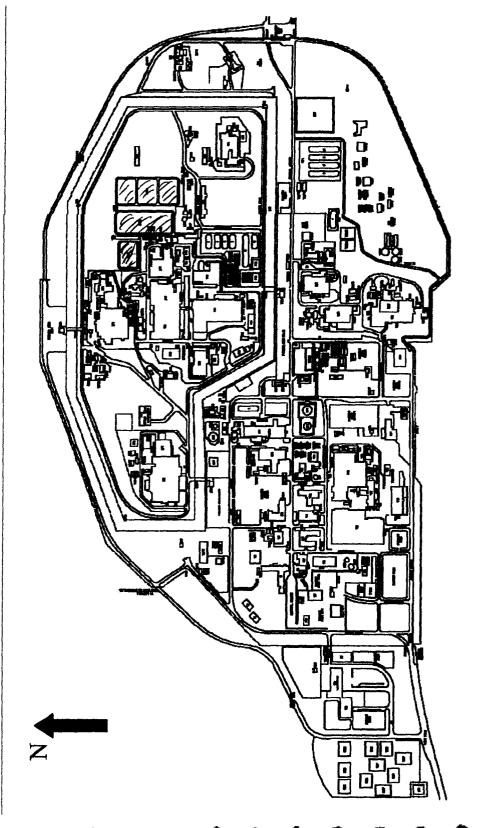
Name	Organization
Greg Choppin	FSU
David Clark	LANL
David Janecky	LANL
Lane Leonard	Tuscon
A J Francis	BNL
Anne Kersting	LLNL
Chris Dayton	K-H
Greg Wetherbee	WWE
lan Paton	WWE
Mike Peters	RMC Consultants
Larry Hersman	LANL
Russell McCallister	DOE/RFFO
Lynn Kıdman	IT-Los Alamos
Chris Hawley	Æ
John Anthony	Parsons
Bruce Curtis	Parsons
Martha Hyder	Radıan
Susan Serreze	Acradia
Laurie Gregory-Frost	E2
Bob Nininger	K-H

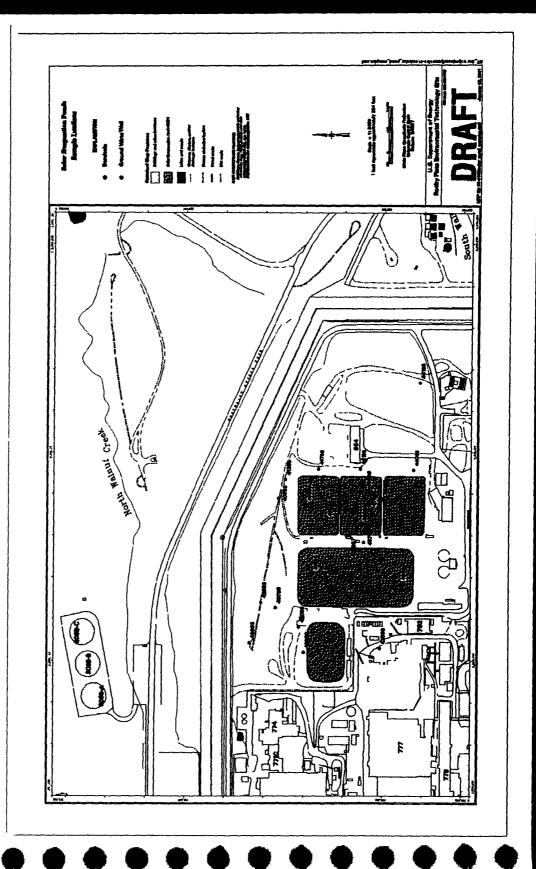
Future Meetings

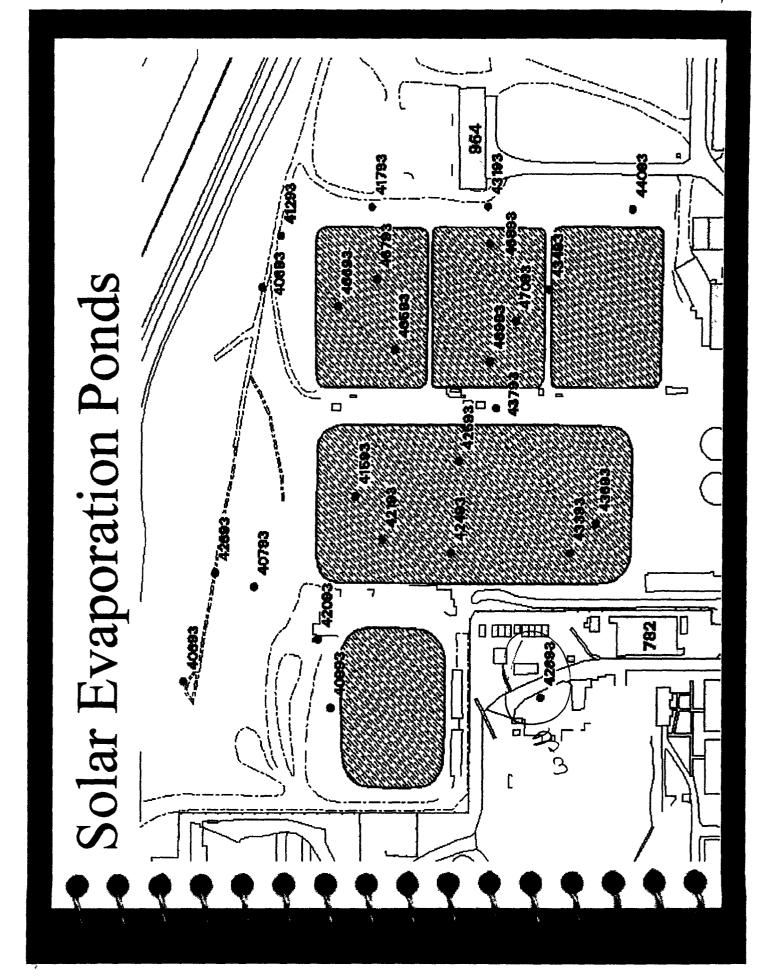
March 27 – advisors conference call April 30-May2 – third quarter Sites meeting July 23-25 – fourth quarter Sites meeting

21

Solar Evaporation Ponds







✓ Uranium analyses for soils and porewater

- Sampled and analyzed in 1993-1994

Analyzed by Mass Spectroscopy (aka TRADS)

- Lysimeters were installed to sample vadose zone porewater

derived from the RFETS Industrial Area Data Summary Report, September 2000 ✓ Suite of analytical data for this study

- Industrial Area Sampling and Analysis Plan ✓ RFETS Industrial Area Data Summary and Comprehensive Risk Assessment Report: Data Quality Filter for the
- For this study only used data identified with the following ratings:
- · "A" quality data passed all filter requirements
- Potential low bias may exist per validation... "UWQ2" is usable data with qualifications.

- ✓ Analytical results compared to RFCA, Attachment 5, Tier I action levels
- No soil results exceeded Tier I action levels (subsurface soil, industrial area land usage)
- exceeded Tier I action levels for groundwater: Porewater samples from three locations 40993, 41593, 43693
- All three area located with current or original solar pond boundaries.

81

Solar Evaporation Ponds

- background soil concentrations (using the background geochemical reports, 1993) ✓ Analytical results compared to RFETS upper tolerance limits identified in the
- background UTLs for highlighted in yellow in tables, e.g., 40693, 40993, 41593, 41793 etc. - Uranium concentration detected above

✓ Soil concentrations range as high as:

– U 233/234: 63.4 pCi/g (46693 SS)

1.689 pCi/g (46693 SS)

– U 235:

- U 238:

25.47 pCi/g (46693 SS)

✓ Porewater concentrations range as high as:

3400 pCi/L (40993) - U 233/234:

120 pCi/L (40993) - U 235:

3700 pCi/L (40993) U 238:

SS = Surface Soil

BH = Borehole = Subsurface Soil

-VE = Porewater

Tolerance Limit for Background Soil ✓UTL = 99% confidence limit Upper Analyses from Rock Creek

KC_Sigma_Error = 2 sigma error

Table C-15 Geologic material UTLs by flow-system for total radionuclides

UPPER TOLERA	NCE LIN	IITS B	Y FLOW-	SYSTEM			
GEOLOGIC MATERIA	LS, TOTAL	RADION	UCLIDES				
	FLOW-	SAMPLE	PERCENT		STANDARD		
ANALYTE	SYSTEM	SIZE, N	DETECTS	MEAN	DEVIATION	UTL 99/99	UNITS
CESIUM-137	LOWER	21	100 00	0 00	0.00	0.00	pCi/g
GROSS ALPHA	LOWER	21	100 00	29 98	8 42	61 78	pCi/g
GROSS BETA	LOWER	21	100 00	25.76	3 85	40.29	pCVg
PLUTONIUM-239,240	LOWER	21	100 00	0.00	0 01	0.03	pCi/g
RADIUM-226	LOWER	14	100.00	109	0 12	163	pCi/g
RADIUM-228	LOWER	14	100.00	1.30	0 19	2.14	pCi/g
STRONTIUM-89,90	LOWER	21	100 00	-0 11	0.36	1.24	pCVg
TRITIUM	LOWER	21	100 00	65.95	122.69	529 32	pCVg
URANIUM, TOTAL	LOWER	21	100 00	1.96	0.64	4 40	pCi/g
UPANIUM-233,234	LOWER	21	100 00	0.96	0 39	2.42	pCi/g
URANIUM-235	LOWER	21	100 00	0.04	0.08	0.35	pCVg
URANIUM-238	LOWER	21	100 00	0 96	0 25	1 92	pCVg
AMERICIUM-241	UPPER	28	100 00	-0 00	0 01	0.02	pCi/g
CESIUM-137	UPPER	99	100 00	0 01	004	011	pCl/g
GROSS ALPHA	UPPER	99	100 00	24 91	9 28	49 48	pCi/g
GROSS BETA	UPPER	99	100 00	2472	606	40 75	pCi/g
PLUTONIUM-239 240	UPPER	99	100 00	0.00	0 01	0.02	pCl/g
RADIUM-226	UPPER	83	100 00	0.75	0 23	1 45	pCl/g
RADIUM-228	UPPER	83	100 00	140	032	2.37	pCl/g
STRONTIUM-89.90	UPPER	99	100 00	0.03	0 36	0.96	pCi/g
TRITIUM	UPPER	99	100 00	141.72	126 75	477 09	pCi/g
URANIUM, TOTAL	UPPER	99	100 00	1 46	079	3.55	pCi/g
URANIUM-233,234	UPPER	99	100 00	078	0 93	3 25	pCi/g
URANIUM-235	UPPER	99	100 00	0.05	0.05	0 14	pCi/g
URANIUM-238	UPPER	99	100 00	073	0 38	1 73	pCl/g

Table C-16. Geologic material UTLs by flow-system for total "water-quality" parameters.

UPPER TOLERAN TOTAL "WATER-QUALIT			Y FLOW-	SYSTEM			
ANALYTE	FLOW- SYSTEM	SAMPLE SIZE, N	PERCENT DETECTS	MEAN	STANDARD DEVIATION	UTL 99/99	UNITS
PH	LOWER	21	100 00	8 43	0 87	11 73	PH UNIT
PH SULFIDE	UPPER UPPER	97 88	100 00 27.27	8 00 2.22	0 69 2.52	9 61 9 88	PH UNIT MG/KG

Analytical Results for Porewater

LOCATION_C = 40793	5 = 40793			Method = TRADS	TRADS			
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VE40726AE	Uranium 238	5/12/93	77	pCi/L	1	0 038	0 46	4

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VEADTOTAE	Frankin 235	5/12/93	101	PC//L	0.0213	- 1	20.5	
VE#0/2/04		00,0	-	2	0.0747		0.000	⋖
VF40727AE	Uranium 238	5/12/93	///	איינים	20.5	ı		

LOCATION_C = 41593) = 41593			Method = TRADS	TRADS			
CUST_SAMP_ NUM	ANALYTE_NAME	COLLECTION	TIER I, Attachment 5, Groundwater Action Levels	UNIT_CODE	RESULT	JNIT_CODE RESULT DETECTIO RC_SIGMA ASWD_	RC_SIGMA ASWD_ _ERROR RATING	ASWD_ RATING
VE40740AE	Uranium 233/234	5/19/93	106	PC/I	214 486	0 0653	9 922	A
VE40740AE	Uranium 235	5/19/93	101	PCI/L		0 0653	0 7031	4
VE40740AE	Uranium 238	5/19/93	768	pCi/L		0 0956	4 913	4

LOCATION_C = 42493) = 42493			Method = TRADS	TRADS			
CUST_SAMP_	ANALYTE_NAME	COLLECTION _DATE	TIER I, Attachment 5, Groundwater Action Levels	UNIT_CODE RESULT DETECTION RC_SIGMA ASWD_ _LIMITERROR RATING	RESULT	DETECTION _LIMIT	RC_SIGMA ASWD_ _ERROR RATING	ASWD_ RATING
VE40739AE	Uranium 233/234	5/19/93	106	PC/L	34.1225	0 0925	1 8348	4
VE40739AE	Uranium 235	5/19/93	101	PC/L	2.034		0 2759	V
VE40739AE	Uranium 238	5/19/93	768	DCIVL	17.5848		1 084	×

LOCATION_C = 42893	C = 42893			Method = TRADS	TRADS			
CUST_SAMP_	ANALYTE_NAME	COLLECTION	TIER I,	UNIT_CODE RESULT DETECTIO RC_SIGMA ASWD_	RESULT	DETECTIO	RC_SIGMA	ASWD_
N O N		DATE	Attachment 5, Groundwater Action Levels			N_LIMIT	ERROR RATING	RATING
VE40725AE	Uranium 233/234	5/18/93	106	pCi/L	8.8	0 093	16	4
VE40725AE	Uranium 235	5/18/93	101	PC!/L	0.12	0 059	0 15	A
VE40725AE	Uranium 238	5/18/93	768	pCi/L	3	0 035	0.8	¥

					1000			
110111001	40400			Method = LIANS	コメンク			
	つりこうすい							_
			- 014	INIT OUR BEGINT DETECTION RC SIGMA ASWU.	PECI T	DETECTIO	AC SIGMA	ASWD_
CINT SAMP	ANALYTE NAME	COLLECTION	ָבְּבְּבְּרָבְיִי	ON! COOL	1000	1		DATING
- 1000 -		DATE	Attachment 5,			Z Z	בט בט בט	
		ı	Groundwater					
			Action Levels					ŀ
		00/07/2	106) () ()	14	031	22	A
VE40729AF	Uranium 233/234	5/16/93	3	102		1000	76.0	4
100000	300	5/19/03	5	OC/L	30.0	3	727	
VE40729AE	Uranium 235	2000		Š	10	0.031	14	< <
VEANTOOAE	Liraniim 238	5/18/93	89/	7	D. /	3	6	<
VE#0/23VE	70000	5/40/03	406	Ş		939	8	<
VE40730AE	Uranium 233/234	20.00	3		90	+	42	⋖
VEADTOOR	I Iraniim 235	5/18/93	101	פור	C.P	-	2	•
VE#0/307E		201001	76.8	νiΩα	186	75	77	<
VE40730AE	Uranium 238	20100	200		No. of the Control of			

								_
				Mathod = TRADS	TRADS			
1 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	<u> </u>			30000				
		_				CITOTITI	AMOIO OU	- CMS
		1401200	ומשוד	INIT CODE RESULT DE LECTIO ROLSIGIAIA ASTRO-	RESULT		というのうと	2
CAMP TOLIC	ANA YTE NAME	COLLECTION				FIRM	EDBOR RATING	RATING
- 1000		DATE	Attachment 5.			Z Z		
2		ָ בְּבְּבְּבְּבְּבְּבְּבְּבְּבְּבְּבְּבְּב						
			Groundwater					_
			ACTION Levels		,		1000	•
		00,00	406	//	732,949	0 2803	20 02/	
TA COLOL TY	1 transism 233/234	5/12/93	3	1,00		ı	4 0070	٥
VE40/097F		00,0	101	<u> </u>	47.2509		4.20/0	
L V COTO: II.	1 Formum 235	5/12/93	5	שממ		ı	0110	<
VE40738AE	Cialitati 200		0.00	/i/c	F 7 29.1		51 9412	<
L 4 COROT LT	Ago minori	5/12/93	80/	אייער	4	ı		
VE40738AE	Calling							

LOCATION_C = 43793) = 43793			Method = TRADS	TRADS				
CHST SAMP	ANAI YTH NAME	COLLECTION	TERI	FINIT	T III T	I AR RESULT	DETECTIO	BC SIGMA	DWSA
MON		DATE	Attachment 5,			QUALIFIER N_LIMIT _ERROR RATING	N_LIMIT	ERROR	RATING
			Groundwater			CODES			
			Action Levels						
VE40736AE	Uranium 233/234	5/19/93	106	PCI/L	=	æ	0 032	18	A
VE40736AE	Uranium 235	5/19/93	101	PC/L	0.7	8	0.032	0 34	∢
VE40736AE	Uranium 238	5/19/93	768	PCI/L	6.5	æ	0 032	13	4
VE40737AE	Uranium 233/234	5/19/93	106	DC//L	0.48	8	0 061	03	4
VE40737AE	Uranium 235	5/19/93	101	DCI/L	0.13	B	960 0	0 15	∢
VE40737AE	Uranium 238	5/19/93	768	PCI/L	0.57	a	0 036	0 32	4

NOTE OF	44003			Method = TRADS	TRADS			
LOCATION C = 44033	1 41000							
							4100	0/4/0
CALLO TO LO	ANIA! VTE NAME	COLLECTION	TER I.	UNIT CODE RESULT DETECTIO HO SIGNA ASWO-	RESULT	DELECTIO	というころにはいる	2
COOL DANK			1	_	_	FIVE - W	aCaau	RATING
N 134		DATE	Attachment 5,					
		1	Groundwater					
			Action i evels					
_			201021			1000	07.0	4
	1,000,000 military	5/18/03	106	ממער	4:	2800	0 43	c
1 VE40/31AE	Oranium 233/234	000			7000	3300	0.078	4
	300 million 1	F/18/03	101	200	ま ろう	2000	200	:
1 VE40731AE	Oranium 200	200			1	7	0.50	₫
7 4 20201 71	Linearium 028	5/18/93	768	PC/L	c.	-	200	
VE40731AE	משנוותנו לאם	2000						

A Analytical Results for Soils

		1					Method = TRADS	TRADS			
1 OCATION C = 40693	C = 40693							-			
_						01001	THE SIGNA ASWO	T III T	PETECTIO	RC SIGMA	ASWO
CINCT CAMP	CLIET CAMP ANALYTE NAME COLLECTION	COLLECTION	SAMPLE	LITHOLOGY	TER I,	מדירם	JON - 1900		FINE	EBOR RATING	PATING
- INCO 1000		DATE	INTERVAL		Attachment 5,						}
WON .		ן ן			Subsurface Soil,	LIMIT, Upper					
					Industrial Use						
						(UTL 99/99)					
					1007	20.0	0/0	2.5	0 0 13	0 42	<
	1000000 miles	20000	525	Ordanic Vill	1020	3.63	l	A LOCAL COLONIAL PROPERTY.	Ī	000	
534005/AE	Uranium 233/234	2007		0	+13	0.14	200	が一般ない	0013	800	<
SCANOSTAR	Uranium 235	2/25/93	0-2 III	Organic Sill			ĺ	The state of the s	0.043	0.36	⋖
	000	CONTRACT	0.0 ln	Consolic Sit	200	1/3	pond	A STATE OF THE PARTY OF THE PAR	ı		
SOAMS TAR	Practition 238	28/27/3	25.30	11000							

LOCATION C = 40793	3 = 40793						Method =	TRADS			
CUST_SAMP_	ANALYTE_NAME	COLLECTION	SAMPLE	LITHOLOGY	Tier I,	UPPER	UNIT_CODE RESULT	RESULT	DETECTIO	RC_SIGMA ASWD	ASWD_
NON NO		DATE	INTERVAL		Attachment 5,	TOLERANCE		-	N_LIMIT	ERROR	RATING
					Subsurface Soil,	LIMIT, Upper		_			
					Industrial Use	Flow System					
						(UTL 99/99)				i	
SS40058AE	Uranium 233/234	2/25/93	0-2 In	Sandy Silt	1627	3.25	5/i⊃d	1.9	0 0 1 1	98 0	4
SS40058AE	Uranium 235	2/25/83	0-2 in	Sandy Silt	113	0 14	5//Od	0 13	0 029	0 084	4
SS40058AE	Uranium 238	2/25/93	0-2 in	Sandy Silt	208	173	p,Od		1100	0.28	4
BH40157AE	Uranium 233/234	3/1/93	25 tt	Sandy Silt	1627	3.25	DCI/Q	ا ا	0 0 1 2	017	4
BH40157AE	Uranium 235	3/1/93	0-6 ft	Sandy Sift	113	0 14	₽C/\g	0 065	0 005	0 032	∢
BH40157AE	Uranium 238	3/1/93	0-6 ft	Sandy Sift	909	173	₽CI/Q	1.2	0 0 1 2	0 16	∢
BH40413AE	Uranium 233/234	3/1/93	0-6 ft	Sandy Sift	1627	3.25	5/IOd	1.5	0 0 1 2	0 19	4
BH40413AE	Uranium 235	3/1/93	0-6 ft	Sandy Silt	113	0 14	5/≀Od	0.068	0 005	0 034	4
BH40413AE	Uranium 238	3/1/93	0-6 ft	Sandy Silt	206	173	6/iOd	-	0 005	0.15	∢
BH40160AE	Uranium 233/234	3/2/93	6-8 1 ft	Sandy Silt	1627	3.25	6/n⊃d	1,3	0 005	0 17	4
BH40160AE	Uranium 235	3/2/93	6-8.1 ft	Sandy Sift	113	0 14	5/Od	0 054	0 0 1 1	0 03	4
BH40160AE	Uranium 238	3/2/93	6-8 1 ft	Sandy Silt	909	173	bC/\d	1.1	0 005	0.15	⋖
BH40414AE	Uranium 233/234	3/2/93	8 1-13 ft	Gravelly Silt	1627	3.25	5/Od	1.2	0 0 1 2	0 16	4
BH40414AE	Uranium 235	3/2/93	8 1-13 ft	Gravelly Silt	113	0 14	6/IOd	0 058	0 005	600	4
BH40414AE	Uranium 238	3/2/93	8 1-13 ft	Gravelly Sift	506	173	bC/\2	1,3	0 0 1 2	0.17	4

	 _		_		_	-	_		_		_
	ASWD	RATING			4	<	4	4	4	4	
	RC_SIGMA	ERROR			0.22	0 028	02	0 158	0 0315	0 142	
	JNIT_CODE RESULT DETECTIO RC_SIGMA ASWD_	N_LIMIT			60 0	0.1	60 0	0 027	0 0 19	0 027	
TRADS	RESULT				60	0 0 1 4	0 82	0 518	0 0091	0 427	
Method = TRADS	UNIT_CODE				DC/\Q	DC/Q	DC//d	D/jOd	B/Od	D/Od	
	UPPER	TOLERANCE	LIMIT, Upper	Flow System (UTL 99/9)	3.25	0 14	173	325	0 14	173	
	TIER I,	Attachment 5,	Subsurface Soil,	Industrial Use	1627	113	506	1627	113	206	
	ПТНОСОВУ				Gravelly Sand	Gravelly Sand	Gravelly Sand	Sandy Gravel	Sandy Gravel	Sandy Gravel	ock
	SAMPLE	INTERVAL			0-2 in	0-2 in	0-2 In	0-7 ft	0-7 ft	0-7 ft	ft = top of bedrock
	COLLECTION	_DATE			12/15/92	12/15/92	12/15/92	12/15/92	12/15/92	12/15/92	63
C = 40893	ANALYTE_NAME				Uranium 233/234	Uranium 235	Uranium 238	Uranium 233/234	Uranium 235	Uranium 238	
LOCATION_C = 40893	CUST_SAMP_	S S S			SS40004AE	SS40004AE	SS40004AE	BH40030AE	BH40030AE	BH40030AE	

	C = 40993						Method =	STATES			
							1000 E		DETECTIO	AMOIS OF	ACWD
CUST_SAMP_	ANALYTE_NAME	COLLECTION	SAMPLE	LITHOLOGY	TIER I.	UPPER	UNITCODE	MESOLI	N IMIT	FROR	RATING
W O N		_DATE	INTERVAL		Subsurface Soil,	LIMIT, Upper					
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,					Industrial Use	Flow System (UTL 99/99)					
7 405-001-00	1,000,000 million	SOROS	0-20 in	Sandy Gravel	1627	3.25	pC//g	2.9	0 0 1 7	0.65	4
5540072AE	Uranium 295	208/03	0-2-1	Sandy Gravel	113	0 14	DCI/G		0 017	0.15	4
SSAUDIZAE	Oranium 200	20000	0.0	Sandy Gravel	206	173	DCI/G	16	0 0 1 7	0 43	4
SS400/ZAE	Uranium 230	20000	200	Sanch Gravel	1627	325	D/Od	2.9	0 093	0 93	4
SS40412AE	Uranium 233/234	2/20/90	100	Sandy Gravel	113	0 14	D/iQa	100	0 035	0.22	4
SS40412AE	Uranium 235	2/20/33	E 70	Sairey Grave	2 2	179	OCI/O	1.2	900	0 53	4
SS40412AE	Uranium 238	2/26/83	440	Cond. City	1807	326	DC/Q	2.7	0 034	0.86	4
BH40201AE	Uranium 233/234	3/3/83	= 0 0	Sandy Grave	Ì	}					
BH40201AF	Uranium 235	3/3/93	0-5 ft	Sandy/Silty	113	0 14	bC//d	0 035	0 0 0 2 2	0 08	DW02
				Sandy Gravel							ŀ
BH40201AE	Uranium 238	3/3/83	0-5 ft	Sandy/Sifty Sandy Gravel	206	173	B/iOd	17	0.034	2 2	₹
DI ACCOUNT	11 Panium 932/934	20,02	6-10 ft	Sandy Gravel	1627	3.25	pC//g	4.2	0 034	05	4
DH40Z04AE	I frankim 235	3/3/93	6-10 ft	Sandy Gravel	113	0 14	bCi/g	0 041	0 034	0 084	4
14000 TH	Communication 238	SAME	A-10#	Sandy Gravel	206	173	pC//g	0.87	0 034	0 42	4
BH40204AE	Uranium 200	20,3/6	10-10#	Silty Sandatone	1627	2 42 (lower flow	pOlyg		0 039	071	⋖
BH40206AE	Oranium 235/254	26.55		layers in Claystone		system)					
BH40206AE	Uranium 235	3/5/83	10-19 ft	Sifty Sandstone tayers in Claystone	113	035	bC//g	800	0 039	860 0	∢
BH40206AE	Uranium 238	3/5/83	10-19 ft	Silty Sandston layers in Claystone	808	192	pCvg	*	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	69 0	∢
BH40415AE	Uranium 233/234	3/5/93	20-29 ft	Silty Sandstone layers in Claystone	1627	2 42	₿/Ŋd	6	0 031	0.5	∢
BH40415AE	Uranium 235	3/5/83	20-29 ft	Silty Sandstone layers in Claystone	113	0.35	B _O /Qd	0.13	0 048	0 11	⋖
BH40415AE	Uranium 238	3/5/83	20-29 #	Sifty Sandstone layers in Claystone	206	1 92	₿/iod		0 0 0 4 8	0 54	∢

LOCATION_C = 40993	C = 40993						Method = TRADS	TRADS			
CUST_SAMP_ NUM	CUST_SAMP_ ANALYTE_NAME COLLECTION NUMDATE	COLLECTION _DATE	SAMPLE	LITHOLOGY	TIER I, Attachment 5, Subsurface Soil, Industrial Use	UPPER TOLERANCE LIMIT, Upper Flow System (UTI 99/89)	UNIT_CODE RESULT DETECTIO RC_SIGMA ASWD_ N_LIMIT _ERROR RATING	RESULT	DETECTIO N_LIMIT	RC_SIGMA ASWD_ _ERROR RATING	ASWD_ RATING
BH40416AE	Uranium 233/234	3/5/93	31-35 ft	Claystone	1627	2.42	pCi/g	980	9900	0 39	4
BH40416AE	Uranium 235	3/5/93	31-35 ft	Claystone	113	0 35	bC/d	7600	0 026	011	4
BH40416AE	Uranium 238	3/5/93	31-35 ft	Claystone	909	1 92	pCVg	-	80 0	0 43	4
		97	9 7 ft = top of bedrock	ock							

LOCATION C = 41293) = 41293						Method = TRADS	TRADS			
CUST_SAMP_ NUM	ANALYTE_NAME COLLECTION _DATE	COLLECTION _DATE	SAMPLE	ПТНОСОВУ	TIER I, Attachment 5, Subsurface Soil, Industrial Use	UPPER TOLERANCE LIMIT, Upper Flow System (UTI 99/89)	UNIT_CODE RESULT DETECTIO RC_SIGMA ASWD_N_LIMIT _ERROR RATING	RESULT	DETECTIO N_LIMIT	RC_SIGMAERROR	ASWD_ RATING
SS40071AE	Uranium 233/234	2/23/93	0-2 in	Sifty Sand	1627	3	DCI/G	-	0 0 12	0.29	4
SS40071AE	Uranium 235	2/23/93	0-2 In	Sifty Sand	113	0 18	D/Od	9900	0 0 12	0 0 7 2	4
SS40071AE	Uranium 238	2/23/93	0-2 in	Sifty Sand	206	19	DCI/Q	=	0 02	0.28	4
BH40196AE	Uranium 233/234	2/23/93	0-3 3 ft	Sandy Gravel	1627	က	pCi/g	1,3	0 031	04	∢
BH40196AE	Uranium 235	2/23/93	0-3.3 ft	Sandy Gravel	113	0 18	DC/\Od	0 038	0 049	0 062	UWQ2
BH40196AE	Uranium 238	2/23/93	0-3 3 ft	Sandy Gravel	206	19	DC//d	1.2	0 0 18	0320	4
			3.3 ft = top of bedrock	edrock						`	

LOCATION C = 41593	C = 41593						Method = TRADS	TRADS			
CUST_SAMP_	ANALYTE_NAME	COLLECTION	SAMPLE	ПТНОСОВУ	TIER I,	UPPER TOI FRANCE	UNIT_CODE RESULT DETECTIO	RESULT	DETECTIO N LIMIT	RC_SIGMA ASWD_ ERROR RATING	ASWD_ RATING
2		1			Subsurface Soil,	LIMT, Upper			,		
					Industrial Use	Flow System					
						(DIL 99/99)					I
		1	0-3 in = asphalt	<u>.</u>				1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			
SS40073AE	Uranium 233/234	4/6/93	4-6 in	No description	1627	3.25	pCi/g		0 0 1 4	17	4
SS40073AE	Uranium 235	4/6/93	4-6 in	No description	113	0 14	bCi/g		0 023	0 14	4
SS40073AE	Uranium 238	4/6/83	4-6 in	No description	909	173	pC//g		0 0 1 4	12	4
BH40417AE	Uranium 233/234	4/6/93	0-2#	No description	1627	325	pCi/g		0 021	2:5	4
BH40417AE	Uranium 235	4/6/93	0-2#	No description	113	0 14	pC//d	200	0 013	02	4
BH40417AE	Uranium 238	4/8/93	0-2 ft	No description	909	173	pC//g		0 021	13	4
				Clayey Silt to							
	;	1		Sandy Silt to	-00,	i c	Ç		000	•	•
BH40418AE	Uranium 233/234	4/6/93	2-4 TI	Sandy Gravel	182/	3.25	200		9500		<
				Clayey Silt to							
			,	Sandy Silt to	•	;	(0,00	;	•
BH40418AE	Uranium 235	4/6/93	2-4 ft	Sandy Gravel	113	0 14	S S S		0.012	410	<
				Clayery Sift to							
				Sandy Silt to						,	
BH40418AE	Uranium 238	4/6/93	2-4 ft	Sandy Gravel	206	173	bCl/g		0 021	0 93	V
BH40419AE	Uranium 233/234	4/6/93	4-6 ft	Silty Sand	1627	3.25	DC/Q		0 023	14	V
BH40419AE	Uranium 235	4/6/83	4-6 ft	Sifty Sand	113	0 14	pCi/g	0	0.014	0.14	¥
BH40419AE	Uranium 238	4/8/93	4-6 #	Silty Sand	909	173	pCi/g		0 0 1 4	0.8	A
BH40424AE		4,6/83	6-7 9 ft	Sandy Siltstone	1627	2 42 (lower)	pCl/g	1.8	0 024	0 42	4
BH40424AE	Uranium 235	4/6/83	6-7 9 ft	Sandy Siltstone	113	035	pCi/g	0 13	0 037	9600	V
BH40424AE	L	4/6/83	6-7 9 ft	Sandy Siltstone	506	1 92	bCl/g	1.2	0014	032	4
			5.9 ft = top of bedrock	bedrock							

LOCATION_C = 41793	5 = 41793						Method = TRADS	TRADS			
CUST_SAMP_ NUM	ANALYTE_NAME	COLLECTION _DATE	SAMPLE	LTHOLOGY	TIER I, Attachment 5, Subsurface Soil, Industrial Use	UPPER TOLERANCE LIMIT, Upper Flow System	UNIT_CODE RESULT DETECTIO	RESULT	DETECTIO N_LIMIT	RC_SIGMA ASWD_ _ERROR RATING	ASWD_ RAŢING
SS40069AE	Uranium 233/234	2/9/93	0-2 in	Sandy Sitt	1627	3.25	DC/Q		0 0717486	0.781	•
SS40069AE	Uranium 235	2/9/83	0-2 in	Sandy Silt	113	0 18		0.07959		0.0677	4
SS40069AE	Uranium 238	2/9/93	0-2 in	Sandy Silt	909	190	D/Qd	7.7		0 496	4
SS40077AE	Uranium 233/234	2/9/93	0-2 in	Sandy Silt	1627	3.25	B/Od	1001	ı	0 642	4
SS40077AE	Uranium 235	2/9/93	0-2 In	Sandy Silt	113	0 18	D/Od	0 1163	1	0 0805	4
SS40077AE	Uranium 238	2/9/93	0-2 in	Sandy Silt	909	1 90	D/Od	2.208	0 0692355	0 464	4
BH40243AE	Uranium 233/234	2/19/93	0-6 ft	Sandy Sift to	1627	3.25	B/Od	.	0 049	0 62	∢
				Sandy Gravel							
BH40243AE	Uranium 235	2/19/83	0-6 ft	Sandy Sift to Sandy Gravel	113	0 18	bC//g	690 0	0 028	960 0	<
BH40243AE	Uranium 238	2/19/93	0-5#	Sandy Sift to Sandy Gravel	906	1 90	₿/JOd	14	0 029	0 52	4
BH40246AE	Uranium 233/234	2/22/93	6-11 ft	Clayey Gravel to Cobbles	1627	3.25	bCi/g	1.2	0 067	0 54	4
BH40246AE	Uranium 235	2/22/83	6-11 ft	Clayey Gravel to Cobbles	113	0 18	₿/i⊃d	0 041	0 067	960 0	UWQ2
BH40246AE	Uranium 238	2/22/93	6-11 ft	Clayey Gravel to Cobbles	909	190	₽Ç/(Q	-	0 04	0 49	∢
		,	12.3 ft = top of bedrock	bedrock							

LOCATION_C = 42093	C = 42093						Method = TRADS	TRADS			
CUST_SAMP_	ANALYTE_NAME	COLLECTION	SAMPLE	ПТНОГОСТ	TIER I,	UPPER	UNIT_CODE RESULT DETECTIO	RESULT		-	ASWD_
Σ Σ			IN EHVAL		Attachment 5, Subsurface Soil,	UMIT, Upper			I W	EHROR	HAHING
					Industrial Use	Flow System (UTL 99/89)					
SS40480AE	Uranium 233/234	1/8/93	0-2 in	Gravelly Sand	1627	325	b/Od	960	01	0.25	4
SS40480AE	Uranium 235	1/8/93	0-2 in	Gravelly Sand	113	0 14	pC//g	0 076	0 1	0 061	4
SS40480AE	Uranium 238	1/8/93	0-2 in	Gravelly Sand	909	172	pC//g	99 0	0.1	0 19	∢
BH40103AE	Uranium 233/234	1/8/93	0-6 ft	Gravelly Sand	1627	325	ø,od		200	0.24	4
				to Sandy		_					
				Gravel to							
BH40103AE	Uranıum 235	1/8/93	0-5#	Gravelly Sand	113	0 14	DC//a	0.047	600	0.048	A
				to Sandy			•	;		?	:
				Gravel to							
				Sandy Clay							
BH40103AE	Uranium 238	1/8/93	# 90	Gravelly Sand	206	172	5/JOd	0 83	200	0 19	¥
				to Sandy				-			
				Gravel to							
4 007 07		9		Sandy Clay							
BH40483AE	Uranium 233/234	1/8/93	# 9 8	Gravelly Sand	1627	325	pC/Q	1 538	0 057	0 359	⋖
				to Sandy							
				Grave to Sandy Clay							
BH40483AE	Uranium 235	1/8/93	0-6 #	Gravelly Sand	113	0 14	bC/\d	0 06142	0 0 4 4	0.0616	4
				to Sandy							
				Gravel to							
				Sandy Clay							_
BH40483AE	Uranıum 238	1/8/93	# 90	Gravelly Sand	206	172	5/Od	0 6473	0.051	0 245	4
			-	to Sandy							
				Gravel to							
				Call Cy Clay							
			4 8 IT = top of begrock	Marock							

	CH 44.180						Method = TRADS	TRADS			
CUST_SAMP_	ANALYTE_NAME	COLLECTION	SAMPLE	ПТНОГОВУ	TIER I,	UPPER	UNIT_CODE RESULT	RESULT		RC_SIGMA	
X 5 2		DATE	INTERVAL		Attachment 5, Subsurface Soil, Industrial Use	TOLERANCE LIMIT, Upper Flow System,			N_UMI	ERROR	RATING
			0-6 in = Asphalt			(2) [2]					
SS40012AE	Uranium 233/234	3/10/93	4-6 in	Asphalt	1627	3.25	DC/Q	2000	0.018	0.87	4
SS40012AE	Uranium 235	3/10/93	4-6 In	Asphalt	113	0 14	DC/Q			6900	•
SS40012AE	Uranium 238	3/10/93	4-6 in	Asphalt	88	173	DC/Q	14.0	O	0.61	•
BH40425AE	Uranium 233/234	3/19/83	0-2#	Gravelly Silt	1627	3.25	DC/\Q			3.1	4
BH40425AE	Uranium 235	3/19/93	0-2#	Gravelly Silt	113	0 14	DC/\Q			0.27	4
BH40425AE	Uranium 238	3/19/93	0-2 ft	Gravelly Silt	909	173	D)Oa	ŧ		17	4
BH40426AE	Uranium 233/234	3/19/83	0-6 ft	Gravelly Silt to Sandy Gravel	1627	3.25	bC/\d	17		0 44	4
BH40426AE	Uranium 235	3/19/93	0-6#	Gravelly Sitt to Sandy Gravel	113	0 14	bCi/g	0 14	0 0 16	0.1	∢
BH40426AE	Uranıum 238	3/19/93	0-6#	Gravelly Silt to Sandy Gravel	206	1 73	pC//g	11	0 049	0 34	∢
BH40427AE	Uranıum 233/234	3/19/83	0.5 #	Gravelly Silt to Sandy Gravel	1627	3.25	pCi/g	=	0 051	0.45	4
BH40427AE	Uranium 235	3/19/83	0-6#	Gravelly Silt to Sandy Gravel	113	0 14	6/2d	986	0 03	0 16	4
BH40427AE	Uranium 238	3/19/83	0-6 ft	Gravelly Silt to Sandy Gravel	506	173	₿/Od	-	0 051	0 46	4
BH40432AE	Uranium 233/234	3/19/93	6-9 9 ft	Sandy Gravel	1627	3.25	pC//g	072	0 021	0.23	4
BH40432AE	Uranium 235	3/19/93	6-9 9 ft	Sandy Gravel	113	0 14	pCi/g	0.1	0 021	0 0 78	4
BH40432AE	Uranium 238	3/19/83	6-9 9 ft	Sandy Gravel	909	173	D/Od	0 83	0 012	0.26	4
BH40086AE	Uranium 233/234	3/30/83	9 9-16 ft	Clayey Sandstone	1627	2 42(lower)	₽CI/g	0.89	900 0	0 17	∢
BH40086AE	Uranium 235	3/30/83	9 9-16 ft	Clayey Sandstone	113	0.35	pCi/g	0 020	900 0	960 0	∢
BH40086AE	Uranium 238	3/30/83	9 9-16 ft	Clayey Sandstone	206	192	₿//Od	-	0 0 16	0 17	4
BH40091AE	Uranium 233/234	3/30/93	16-22 ft	Claystone	1627	2 42	DC//Cd	0.78	0 007	0.15	4
BH40091AE	Uranium 235	3/30/83	16-22 ft	Claystone	113	0 34	DC/Q	0 023	0 007	0 024	A
BH40091AE	Uranium 238	3/30/83	16-22 ft	Claystone	909	1 92	D/Od	_	0 007	0 18	A
BH40430AE	Uranium 233/234	3/30/83	22-28.3 ft	Interbedded	1627	2 42	₽C/Q	0.83	0 007	0 15	4
				sultatone and claystone							
BH40430AE	Uranium 235	3/30/83	22-28.3 ft	Interbedded	113	034	D _V Od	0.021	0 029	0 026	4
				clavstone							

LOCATION C = 42193	C = 42193						Method = TRADS	TRADS			
CUST_SAMP_	ANALYTE_NAME	COLLECTION	SAMPLE	ПТНОГОВУ	TIER I,	UPPER	UNIT_CODE RESULT DETECTIO	RESULT		RC_SIGMA ASWD_	ASWD
S S		_DATE	INTERVAL		Attachment 5,	TOLERANCE			N_LIMIT	EHROR	RATING
					Subsurface Soil,	LIMIT Upper			-		
					Industrial Use	Flow System, (UTL 99/99)					
BH40430AE	Uranium 238	3/30/93	22-28 3 ft	Interbedded	206	192	pCi/g	0 94	0 024	0 17	∢
				sultstone and clavstone							
BH40433AE	Uranium 233/234	3/31/93	28 3-31 3 ft	Interbedded	1627	2 42	D/Qd	-	0000	0.18	4
				claystone and clayey siltstone						!	
	-	9									
BH40433AE	Uranium 235	3/31/83	78 3-31.3 T	Interbedded claystone and	113	0 34	6/iod	0 0 0 0	0 000	0 034	∢
				ciayey siltatone							
BH40433AE	Uranium 238	3/31/93	28 3-31 3 ft	hebbedretni	909	1 92	bciva	:	2000	0 18	A
				daystone and				-			
				dayey ontothe							
			7 4 ft = top of bedrock	edrock							

LOCATION_C = 42493	= 42493						Method = TRADS	TRADS			
CUST_SAMP_	ANALYTE_NAME	COLLECTION _DATE	SAMPLE	итногову	TIER I, Attachment 5, Subsurface Soil, Industrial Use	UPPER TOLERANCE LIMIT, Upper Flow System (UTL 99/89)	UNIT_CODE RESULT	RESULT	DETECTIO N_LIMIT	RC_SIGMAERROR	ASWD_ RATING
			0-6 in = Asphalt								
CCANORAGE	Hranum 233/234	3/8/93		Gravelly Sand	1627	3.25	DCiva	1.2	0 005	0 17	∢.
SCACOBOATE TACADOS	I frantim 235	3/8/93	6-7 in	Gravelly Sand	113	0 14	bC/g	0 038	0 005	0 024	∢.
SCANOBOAE CCANOBOAE	I francis 238	3/8/93	5-7 in	Gravelly Sand	206	173	bCi/g	-	0 005	0 15	4
BH40438AE	Uranium 233/234	3/23/93	0-2 ft	Gravelly Sand to Silty Gravel	1627	3.25	pCi/g		0 0 19	0 82	<
BH40438AE	Uranium 235	3/23/83	0-2#	Gravelly Sand to Silty Gravel	113	0 14	₿/iod		0 032	0 17	∢
BH40438AE	Uranium 238	3/23/93	0-2#	Gravelly Sand to Silty Gravel	208	1 73	bCi/g		0 032	0 54	∢
BH40112AE	Uranium 233/234	3/23/93	ī	Gravelly Sand to Silty Gravel to Sandy Gravel	1627	325	bCv(g	.	0 0 19	0 45	⋖
BH40112AE	Uranum 235	3/23/93	4	Gravelly Sand to Silty Gravel to Sandy Gravel	113	0 14	₿/iOd	6900	0 0 0 1 9	80 0	∢
BH40112AE	Uranium 238	3/23/93	1	Gravelly Sand to Silty Gravel to Sandy Gravel	208	173	b⊘v3	0.76	0 019	0.29	∢
BH40439AE	Uranium 233/234	3/23/93	4 #	Gravelly Sand to Silty Gravel to Sandy Gravel	1627	3.25	5/i⊙d	091	0 083	0 38	∢
BH40439AE	Uranium 235	3/23/83	1	Gravelly Sand to Silty Gravel to Sandy Gravel	113	0 14	₿ BOI/₫	0.14	0 024	0 13	∢
BH40439AE	Uranium 238	3/23/83	<u>1</u>	Gravelly Sand to Silty Gravel to Sandy Gravel	909	173	₿/iOd	1.3	0 024	0 44	∢
BH40440AE	Uranıum 233/234	3/23/83	# 90	Gravelly Sand to Sity Gravel to Sandy Gravel	1627	3.25	₿//Od	0.97	0 021	0 35	4

LOCATION C = 42493	C = 42493						Method = TRADS	TRADS			
CUST_SAMP_	ANALYTE_NAME	COLLECTION	SAMPLE	LITHOLOGY	TERI	UPPER	UNIT_CODE	RESULT	UNIT_CODE RESULT DETECTIO RC_SIGMA ASWD	RC_SIGMA	ASWD
WON.		DATE	INTERVAL		Attachment 5,	TOLERANCE	1		N	ERROR	RATING
					Subsurface Soil,	LIMIT, Upper					
					Industrial Use	Flow System					
						(UTL 99/89)					
BH40440AE	Uranium 235	3/23/93	0-5 ft	Gravelly Sand	113	0 14	B/jQd	011	0 064	0 11	4
				to Sifty Gravel							
				to Sandy							
BH40440AE	Uranium 238	3/23/93	0-6 ft	Gravelly Sand	506	173	DCI/a	-	0.054	0.38	A
		-		to Silty Gravel			•			}	:
				to Sandy			-				
				Gravel					-		
BH40441AE	Uranium 233/234	3/23/93	4-8 ft	Sandy Gravel	1627	3.25	S/Od	0 84	0 0 18	03	4
BH40441AE	Uranium 235	3/23/93	4-8 ft	Sandy Gravel	113	0 14	B/jQd	9800	0 0 18	0 086	4
BH40441AE	Uranium 238	3/23/93	4-8 ft	Sandy Gravel	909	173	5/jQd	990	0 03	0.26	4
BH40445AE	Uranium 233/234	3/23/93	8-10.2 ft	Sandy Siltstone	1627	2 42 (lower)	Ş	-	0 02	0.35	4
BH40445AE	Uranium 235	3/23/93	8-10.2 ft	Sandy Sittstone	113	0.35	DANCE	0.047	0 02	0 068	4
BH40445AE	Uranium 238	3/23/93	8-10.2 ft	Sandy Siltstone	206	192	D/jQd	890	0 02	0.28	A
			8 1 ft = top of bedrock	edrock							
								1			

LOCATION_C = 42593	C = 42593						Method =	TRADS			
CUST_SAMP_	ANALYTE_NAME	COLLECTION	SAMPLE	LITHOLOGY	TIER I,	UPPER	UNIT_CODE RESULT	RESULT	DETECTIO		ASWD_
		1			Subsurface Soil,	LIMIT, Upper				רטבעם	5
					Industrial Use	Flow System (UTL 99/99)					
			0-6 in = Asphalt								
SS40082AE	Uranium 233/234	3/9/93		Sandy Gravel	1627	3.25	D/O		0 041	12	A
SS40082AE	Uranium 235	3/9/93	4-6 in	Sandy Gravel	113	0 14	bCiva	8	0	0 105	A
SS40082AE	Uranium 238	3/9/83	46 in	Sandy Gravel	909	1 73	pCi/o		0	071	4
BH40446AE	Uranium 233/234	3/16/83	0-2 ft	Sandy Gravel	1627	3.25	pCi/g		0 033	2	4
BH40446AE	Uranium 235	3/16/93	0-2 ft	Sandy Gravel	113	0 14	DC/Q		0 0 19	0 16	V
BH40446AE	Uranium 238	3/16/93	0-2 ft	Sandy Gravel	909	173	BC/Q	618	0 033	13	4
BH40447AE	Uranium 233/234	3/16/93	Į,	Sandy Gravel	1627	3.25	pCi/g	-	0 038	0.28	V
BH40447AE	Uranium 235	3/16/93	410	Sandy Gravel	113	0 14	pCi/g	0 044	0 0 1 2	0 052	4
BH40447AE	Uranium 238	3/16/93	44	Sandy Gravel	206	1 73	pC//g	28 0	0 021	0.25	<
BH40448AE	Uranium 233/234	3/16/93	95#	Sandy Gravel	1627	3.25	pCi/g	1.5	0 021	98 0	4
BH40448AE	Uranium 235	3/16/93	06 ft	Sandy Gravel	113	0 14	pCi/g	0 075	0 013	9900	4
BH40448AE	Uranium 238	3/16/93	0-5#	Sandy Gravel	909	1 73	DC/\d	17	0 013	0 38	4
BH40449AE	Uranium 233/234	3/16/93	4-8 #	Sandy Gravel	1627	3.25	pCi/g	1.2	0 021	031	4
BH40449AE	Uranium 235	3/16/93	4-8 ft	Sandy Gravel	113	0 14	DCI/Q	200	0 033	9900	<
BH40449AE	Uranium 238	3/16/93	4.8 tt	Sandy Gravel	803	173	pCi/g	1.3	0 0 1 2	0 32	K
BH40450AE	Uranium 233/234	3/16/93	8-10 ft	Silty Claytone	1627	2 42 (lower)	pCi/g	1.2	0 031	031	<
BH40450AE	Uranium 235	3/16/83	8-10 ft	Sifty Claytone	113	0.35	pCi/g	0.071	0 0 1 2	0 064	<
BH40450AE	Uranium 238	3/16/83	8-10 ft	Silty Claytone	88	1 92	pCi/g	0 92	0 02	0.26	4
BH40290AE	Uranium 233/234	3/26/83	10 2-16.8 ft	Sandy Sittstone	1627	2.42	pC//g	0.84	9000	0 16	4
BH40290AE	Uranium 235	3/26/83		Sandy Siltstone		0 35	5/Od	0.031	0 025	0 03	4
BH40290AE	Uranium 238	3/26/83	10 2-16.8 ft	Sandy Sittstone	206	1 92	bCi/g	0.89	9000	0 17	<
			80 ft = tip of bedrock	adrock							

TOACH TOACH	Method a boundary		T	TIER I, UPPER UNIT COUR MESULI D	Attachment 5. TOLERANCE N_LIMIT	Subsurface Soil.		1007	A SA	112 0019 0031		22 0043
				LI BINDS NOTO	THE PART OF THE PA	DAIE INIERVAL	 	1	0-2 ln 0		2202 0-2 in C	
		# 42023		1100	NALY IE NAME COL		 		L	Uranium 233/234	_	CCS LINES
		LOCATION C = 42683			J M M	NO.				SS40080AE		SSACOROAE

LOCATION C = 43193	C = 43193						Method - TDADS	TDANG			
							30110111				
CUST_SAMP_	ANALYTE_NAME	COLLECTION	SAMPLE	LITHOLOGY	TIER I,	UPPER	UNIT CODE	RESULT	DETECTIO	JNIT CODE BESULT DETECTIO RC SIGMA ASWD	ASWD
N N		_DATE	INTERVAL		Attachment 5,	TOLERANCE			LMI	ERROR RATING	RATING
					Subsurface Soil,	LIMIT, Upper				1	
	-				Industrial Use	Flow System (UT) 99/99)					
SS40084AE	Uranium 233/234	2/9/93	0-2 in	Sandy Gravel	1627	3.25	DO/Q	1 500	0.0644476	0330	•
SS40084AE	Uranium 235	2/9/83	0-2 Jn	Sandy Gravel	113	0.14	900	0.07494		Ĺ	<
SS40084AE	Uranium 238	2/9/93	0-2 in	Sandy Gravel	505	1 73			0 000000	0,0010	(
BH40306AE	Uranium 233/234	2/12/83	95	Sandy Gravel	1607	200		本 () () () () () () () () () (- 1	1/80	<
BH40306AF	Ilranium 235	2/12/02	96.	Compt. Order	300	0.60	3	-	4100	0.29	4
140000110		20/31/3	3	Call Col Col Col Col	113	0 14	D D D	0 087	0 0 1 4	800	<
DIA0300AE	Uranium 238	2/12/93	0-5#	Sandy Gravel	900	173	D/\(\)	1-1	0.014	0.31	4
BH40309AE	Uranium 233/234	2/15/93	6-11 #	Gravelly Sand	1627	3.25	ν/Ος Ο	0	8000	0.80	
BH40309AE	Uranium 235	2/15/93	6-11 ft	Gravelly Sand		0.14		2000	9000	900	<
BH40309AE	Uranium 238	2/15/93	6-11#	Gravelly Sand		173	200	3	0000	800	<
		101	10 5 ft = ton bedrock	35		2	200		0.000	900	<

LOCATION_C = 43393	C ≈ 43393						Method = TRADS	TRADS			
CUST_SAMP_	ANALYTE_NAME	COLLECTION	SAMPLE	ПТНОСОВУ	TIER 1,	UPPER	UNIT_CODE RESULT		DETECTIO	-	ASWD_
W D N		DATE	DEPTH		Attachment 5, Subsurface Soil,	TOLERANCE LIMIT, Upper			LIMIT N	ERROR	RATING
					Industrial Use	Flow System					
						(UTL 99/99)					
		ò	0-0 5 ft = Asphall	Ħ							
SS40087 AE	Uranium 233/234	3/8/83	4-6 In	Gravelly Sand	1627	3.25	bC/\0	1 95	0 027	0.47	4
SS40087AE	Uranium 235	3/9/93	4-6 in	Gravelly Sand	113	0 14	5/IOd	0 0745	0 0 18	66300	4
SS40087AE	Uranium 238	3/9/93	4-6 in	Gravelly Sand	206	173	bCi/g	1 42	0 0 18	98 0	∢
BH40510AE	Uranium 233/234	3/18/93	0-2 ft	Sandy Gravel	1627	3.25	pCv2		0 036	081	¥
BH40510AE	L	3/18/83	0-2 ft	Sandy Gravel	113	0 14	bCi/g	9800	0 0 1 2	200	4
BH40510AE	L	3/18/93	0-2 ft	Sandy Gravel	206	173	bCi/g		0 0 1 2	0.74	V
BH40511AE	Uranium 233/234	3/18/93	0-4 ft	Sandy Gravel	1627	3.25	pCI/g	2.2	0 08	250	V
BH40511AE	Uranıum 235	3/18/93	0-4 ft	Sandy Gravel	113	0 14	pCi/g	0 086	0 049	0 082	∢
BH40511AE	Uranium 238	3/18/93	0-4 ft	Sandy Gravel	206	1 73	pCt/g	2.3	0 0 19	0 58	∢
BH40512AE	Uranium 233/234	3/18/93	04 ft	Sandy Gravel	1627	3.25	pCi/g	•	001	0.65	¥
BH40512AE		3/18/93	04 ft	Sandy Gravel	113	0 14	pCi/g	0.14	0 0 18	0 084	¥
BH40512AE	Uranium 238	3/16/93	0-4 ft	Sandy Gravel	206	173	pCl/g	•	0.018	0 52	⋖
BH40517AE	Uranium 233/234	3/18/93	5.4-7.6 ft	Silty Claystone	1627	2 42 (lower)	pCi/g		0 022	0.51	4
BH40517AE	Uranium 235	3/18/93	54-76 ft	Silty Claystone	113	0 35	pCi/g	0 13	0 013	0 092	4
BH40517AE	Uranıum 238	3/18/83	5.4-7.6 ft	Silty Claystone	909	1 92	pCi/g	100 m	0 0 13	0.47	4
BH40324AE	Uranium 233/234	3/18/93	7 6-12.6 ft	Silty Claystone	1627	2 42	pCi/g	-	0.048	034	4
BH40324AE	Uranium 235	3/18/93	7.8-12.8 ft	Sifty Claystone	113	0 35	pCi/g	0 088	0 0 18	0 00	4
BH40324AE	Uranium 238	3/18/93	7 6-12.6 ft	Silty Claystone	909	1 92	pCi/g	17	0 031	0.46	4
		50ft=	ft = top of bedrock	ock							

		40.400					Method = TRADS	TRADS					
LOCATION C=		25455											
CUST_SAMP_	CUST_SAMP_ COLLECTION	CAS_NO	SAMPLE	LITHOLOGY	TIER I,	UPPER	UNIT_CODE RESULT DETECTIO RC_SIGMA VALIDATION	RESULT	DETECTIO N_LIMIT	RC_SIGMA _ERROR	CSIGMA VALIDATION CEROR COUALIFIER	ANALYTE_NAME	RATING
¥ S	DATE		A V H I I		Subsurface Soil,	LIMIT, Upper					3000		
					Industrial Area	(UTL 99/99)							
				Apple	1827		SCIVE	1 52	0 0722999	0 352	V	Uranium 233/234	
SS40086AE	4/21/93	11:08-5	U.7.1	ASDIEN	450		Ş	0.04783	0.0646883	0 0538	4	Uranium 235	4
SS40086AE	4/21/93	15117-96-1	0-2 in	Asprair	2 2		Ş		0 101478	0.265	4	Uranium 238	4
S\$40086AE	4/21/93	7440-61-1	0-2 in	Aspnair	300	30.0	Ş	0 9911	0.0595073	0.252	4	Uranium 233/234	4
BH40319AE	4/21/93	11-08-5	05-5311	Sandy Gravel	70.	27.0	200	OCACA	O 0838043	0.0583	4	Uranium 235	¥
BH40319AE	4/21/93	15117-96-1	05-53ft	Sandy Grave	1	1	300	000	0.0710127	0.248	4	Uranium 238	A
BH40319AE	4/21/93	7440-61 1	05-53#	Sandy Grave		200		0 8843	0 8843 0 0830896	0.238	4	Uranium 233/234	¥
BH40573AE	4/21/83	11-08-5	05-53ft	Sandy Grave		3.53	7	0 00534	0.02831 0.0508432	0.0434	4	Uranium 235	V
BH40573AE	4/21/93	15117-96-1	05-53#	Sandy Grave		4.0	2 2	2010	0.0506430	222	4	Uranium 238	4
BH40573AE	4/21/93	7440-61-1	0.5-5.3 ft	Sandy Gravel		200	200	0000		1	4	Uranium 233/234	V
BH40322AE	4/21/93	11-08-5	53-103	Sandy Gravel		25.0	3 2	0.08235		L	4	Uranium 235	V
BH40322AE	4/21/93	15117-96-1	53-103	Sandy Gravel		100	S S	0 788	0.0807325	0.227	4	Uranium 238	4
BH40322AE	4/21/83	7440-61 1	53-103	Sandy Grave		20.0	2	0 07423	0.247816	0 14	4	Uranium 233/234	4
BH40575AE	4/22/93	11 08-5		Sandy Grave		0.44	2	A 0078	0 198927	0 0111	4	Uranium 235	4
BH40575AE	4/22/93	15117-96-1		Sanoy Grave		2 2	Ş	0030	0 179366	0 00783	4	Uranium 238	4
BH40575AE	4/22/93	7440-61-1		Sandy Gravel	8								
				(entire borehol	rehole is Sandy Gravel								

LOCATION_C = 43693	C = 43693						Method = TRADS	TRADS			
CUST_SAMP_	ANALYTE_NAME	COLLECTION	SAMPLE	ПТНОГОВУ	TIER I,	UPPER	UNIT_CODE RESULT	RESULT	DETECTIO	RC_SIGMA	ASWD_
		!			Subsurface Soil,	LIMIT, Upper				בסיים -	
						(UTL 99/99)					
)	0-6 in = Asphal	-							
SS40089AE	Uranium 233/234	3/10/83	4-6 in	Sandy Gravel	1627	3.25	DOG	2.14	0 02	0 52	<
SS40089AE	Uranium 235	3/10/93	4-6 In	Sandy Gravel	113	0 14	D/Od	0 0841	0 02	0 0584	\
SS40089AE	Uranium 238	3/10/93	4-6 in	Sandy Gravel	909	173	D/Qd	2.21	0 02	0 53	4
BH40518AE	Uranium 233/234	3/24/93	0-2 ft	Sandy Gravel	1627	3.25	D/JOd		0 020056	0 533	<
BH40518AE	Uranium 235	3/24/83	0-2 ft	Sandy Gravel	113	0 14	5/Od		0 0213394	0 0 44	4
BH40518AE	Uranium 238	3/24/93	0-2 ft	Sandy Gravel	909	1 73	bC/Qd		0 0 1 8 6 3 6 4	0 643	4
BH40519AE	Uranium 233/234	3/24/83	1	Sandy Gravel	1627	3.25	g/Qd		0 0176228	0 421	<
BH40519AE	Uranium 235	3/24/93	4	Sandy Gravel	113	0 14	DC!/C	0 1128	0 0130661	0 0356	4
BH40519AE	Uranium 238	3/24/93	Į	Sandy Gravel	206	1 73	bC/∕g		0 0 1 7 6 2 2 8	0 425	4
BH40520AE	Uranium 233/234	3/24/93	0-5 ft	Sandy Gravel	1627	3.25	pCi/g		0 0216164	0 371	V
BH40520AE	Uranium 235	3/24/83	05 #	Sandy Gravel	113	0 14	pCi/g	0 0767	0 0203163	0 0297	4
BH40520AE	Uranium 238	3/24/93	05 ft	Sandy Gravel	909	1 73	5/IOd	\	0 0 1 8 8 7 8 3	0.295	4
BH40521AE	Uranium 233/234	3/25/93	484	Sendy Gravel	1627	3.25	pCi/g	22	0 0 18	0 55	4
BH40521AE	Uranium 235	3/25/93	6-8 ft	Sandy Gravel	113	0 14	5/ı∕d	0 12	0 03	0 11	<
BH40521AE	Uranium 238	3/25/93	£8.4	Sandy Gravel	909	1 73	bCi/g		0 0 18	0 62	4
BH40522AE	Uranium 233/234	3/25/93	8-10 ft	Sandy Gravel	1627	3.25	pCi/g		0 033	-	4
BH40522AE	Uranium 235	3/25/83	8-10 ft	Sandy Gravel	113	0 14	bCl∕g		0 02	0 16	<
BH40522AE	Uranium 238	325/83	8-10 ft	Sandy Gravel		173	pCi/g		0 033	-	<
BH40525AE	Uranium 233/234	3/25/83	10-13 ft	Silty Claystone		2 42 (lower)	pCi/g	15	0 021	0.46	4
BH40525AE	Uranium 235	3/25/83	10-13 ft	Sifty Claystone		0 35	DCI/O	900	0 021	0 072	4
BH40525AE	Uranium 238	3/25/83	10-13 ft	Sifty Claystone		1 92	5/iOd	*	0 021	440	4
BH40563AE	Uranium 233/234	3/25/83	10-13 #	Silty Claystone		2.42	pCi/g	1.5	0 038	0.47	V
BH40563AE	Uranium 235	3/25/83	10-13 ft	Sifty Claystone		0 35	bCi/g	0.21	0 059	0 16	4
BH40563AE	Uranium 238	3/25/83		Sifty Claystone	206	1 92	DCi/g	15	0 022	0 47	4
			10 0 ft = top of bedrock	bedrock							

LOCATION_C = 43793	C = 43793						Method = TRADS	TRADS			
CUST_SAMP_	ANALYTE_NAME	COLLECTION	SAMPLE	ПТНОГОВУ	TIER I,	UPPER	UNIT_CODE RESULT DETECTIO RC_SIGMA ASWD	RESULT	DETECTIO	RC_SIGMA	ASWD_
Š		DATE	INTERVAL		Attachment 5,	TOLERANCE			N	ERROR RATING	RATING
					Subsurface Soil,	LIMIT, Upper				· _	
					Industrial Use	Flow System (UTL 99/99)					
SS40088AE	Uranium 233/234	2/12/93	0-2 in	Gravel	1627	3.25	g/jQd		0 037	16	4
SS40088AE	Uranium 235	2/12/93	0-2 in	Gravel	113	0 14	0/Qd		0 037	0 33	4
SS40088AE	Uranium 238	2/12/93	0-2 in	Gravel	506	173	BOIG		0 062	14	4
BH40332AE	Uranium 233/234	2/23/83	26 #	Gravel to	1627	3.25	SCI/O		0 02	24	4
				Sandy Gravel)				
BH40332AE	Uranium 235	2/23/83	0-6 M	Gravel to	113	0 14	pCi/a		0 012	0 19	4
				Sandy Gravel							
BH40332AE	Uranium 238	2/23/93	£ \$4	Gravel to	206	173	DC/\d		0 012	0 94	4
				Sandy Gravel)				
BH40335AE	Uranıum 233/234	2/24/93	6-115ft	Sandy Gravet	1627	3.25	D/Q	11	0 054	0.47	4
BH40335AE	Uranium 235	2/24/93	6-11.5 ft	Sandy Gravel	113	0 14	o So So So	-0 005	0 054	0 001	UWQ2
BH40335AE	Uranium 238	2/24/93	6-11 5 ft	Sandy Gravel	206	173	g/Qa	072	0 054	0.36	4
		113ft=	ft = top of bedrock	rock							

LOCATION_C = 44093	C = 44093						Method = TRADS	TRADS			
CUST_SAMP_	ANALYTE_NAME	COLLECTION	SAMPLE	ПТНОГОВУ	TIER I,	UPPER	UNIT_CODE RESULT DETECTIO	RESULT	DETECTIO	RC_SIGMA ASWD	ASWD_
Ž N		DATE	INTERVAL		Attachment 5,	TOLERANCE			LIMIT	ERROR	RATING
			-		Subsurface Soil,	LIMIT, Upper					
					Industrial Use	Flow System					
SS40090AE	Uranium 233/234	2/9/93	0-2 in	Sandy Silt	1627	3.25	DC/Q	0.91	0 014	0.28	4
SS40090AE	Uranium 235	2/9/93	0-2 ln	Sandy Silt	113	0 14	D/Oa	0 065	0 024	0.068	4
SS40090AE	Uranium 238	2/9/93	0-2 in	Sandy Silt	200	173	, p/Q	0 78	0 0 1 4	0.25	<
BH40348AE	Uranium 233/234	2/9/93	96 ft	Silty Sand to	1627	325	ρχα	0 78	0.05	0.26	A
				Silty Gravel	-			,	}		
BH40348AE	Uranium 235	2/9/93	0-6 ft	Silty Sand to	113	0 14	D/JQd	0 017	0 0 1 4	0 0 34	
				Silty Gravel							
BH40348AE	Uranium 238	2/9/93	5	Silty Sand to	206	173	D/\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	0 83	0 057	0.27	4
				Silty Gravel							
BH40351AE	Uranium 233/234	2/10/93	6-10.4 ft	Sandy Gravel	1627	3.25	DÇI/Q	0 5887	0.0511965	0 189	\
BH40351AE	Uranium 235	2/10/83	6-10 4 ft	Sandy Gravel	113	0 14	βÖĞ	0 02413	0 02413 0 0461623	0 0357	4
BH40351AE	Uranium 238	2/10/93	6-10 4 ft	Sandy Gravel	206	173	5/ 0⁄2	0 5625	0 0550594	0 185	4
		1141	ft = top of bedrock	rock							

<u> </u>	LOCATION C = 44193	C = 44193						Mathod	TDADO			
ANALYTE_NAME COLLECTION SAMPLE LITHOLOGY TIER I, TOLERANCE UNIT_CODE RESULT Uranium 239/234 12/1892 0-2 in Sandy Gravel 113 0 14 PCVg 0 699 Uranium 239/234 12/1892 0-2 in Sandy Gravel 113 0 14 PCVg 0 699 Uranium 239 12/1892 0-2 in Sandy Gravel 153 0 14 PCVg 0 699 Uranium 239 12/1892 0-2 in Sandy Gravel 153 0 173 0 690 0 691 Uranium 239 12/21/92 0-6 ft Sandy Gravel 153 0 691 0 691 0 691 Uranium 238 12/21/92 0-6 ft Sandy Gravel 153 0 691 0 691 0 691 Uranium 238 12/21/92 0-6 ft Sandy Gravel 150 0 691 0 691 0 691 Uranium 238 12/21/92 0-6 ft Sandy Gravel 153 0 692 0 74 0 691 0 691 Uranium 238 12/21/92												
Uranium 233/234 12/18/32 O-2 in Sandy Gravel Titre 1, 10 PPER (ILMT_CODE RESULT) UNIT_CODE RESULT Uranium 233/234 12/18/32 0-2 in Sandy Gravel 1627 3.25 DC/g 0 634 Uranium 236 12/18/32 0-2 in Sandy Gravel 113 0 14 DC/g 0 634 Uranium 236 12/18/32 0-6 ft Sandy Gravel 113 0 14 DC/g 0 634 Uranium 236/234 12/21/82 0-6 ft Sandy Gravel 113 0 14 DC/g 0 634 Uranium 236/234 12/21/82 0-6 ft Sandy Gravel 113 0 14 DC/g 0 641 Uranium 236 12/21/82 0-6 ft Sandy Gravel 113 0 14 DC/g 0 641 Uranium 238 12/21/82 0-6 ft Sandy Gravel 113 0 14 DC/g 0 641 Uranium 238 12/21/82 0-12 ft Sandy Gravel 150 0 14 DC/g 0 641 Uranium 238 12/21/82 0-12 ft Sandy Gravel 160 1 74 DC/g 0 14 Uranium 238	CUST_SAMP_	ANALYTE NAME	COLLECTION	SAMDIE	VAC IOUT!							
Uranium 239.234 12/18/92 0-2 in Sancy Gravel Flow System Flow System Uranium 239.234 12/18/92 0-2 in Sancy Gravel 113 0.14 DC/g 0.689 Uranium 239. 12/18/92 0-2 in Sancy Gravel 113 0.14 DC/g 0.689 Uranium 239.234 12/18/92 0-2 in Sancy Gravel 1627 3.25 DC/g 0.691 Uranium 239.234 12/21/92 0-6 ft Sancy Gravel 1627 3.25 DC/g 0.691 Uranium 239.234 12/21/92 0-6 ft Sancy Gravel 1627 3.25 DC/g 0.691 Uranium 239.234 12/21/92 0-6 ft Sancy Gravel 1627 3.25 DC/g 0.691 Uranium 239.234 3/21/92 0-12 ft Sancy Gravel 1627 2.42 DC/g 0.691 Uranium 239.234 3/21/93 2-2-24.4 Claystone 113 0.35 DC/g 0.691 Uranium 239 3/21/93 2-2-24.4	NC N	ļ	DATE		ביים ביים	Į.	UPPER	UNIT_CODE	RESULT	DETECTIO	RC SIGMA ASWD	ASWD
Uranium 239/234 12/18/92 O-2 in Sandy Gravel 1627 3.25 DClyg 0.69			ב כ כ	INTERNAL		Attachment 5,	TOLERANCE			N I MAIT	2002	
Uranium 239/234 12/18/92 0-2 in Sandy Gravel 1627 3.25 pCuig 0.68 Uranium 239 12/18/92 0-2 in Sandy Gravel 113 0.14 pCuig 0.68 Uranium 235 12/18/92 0-2 in Sandy Gravel 150 0.14 pCuig 0.74 Uranium 238/234 12/21/82 0-6 ft Sandy Gravel 1627 3.25 pCuig 0.74 Uranium 238/234 12/21/82 0-6 ft Sandy Gravel 166 173 pCuig 0.69 Uranium 238/234 12/21/82 0-6 ft Sandy Gravel 506 173 pCuig 0.69 Uranium 238 12/21/82 0-12 ft Sandy Gravel 506 173 pCuig 0.69 Uranium 238 12/21/82 0-12 ft Sandy Gravel 506 173 pCuig 0.69 Uranium 238 3/31/83 23 4-29 4ft Claystone 152 2.42 pCuig 0.69 Uranium 238 3/31/83 23 4-36						Subsurface Soil,	LIMIT, Upper				בייייייייייייייייייייייייייייייייייייי	2
Uranium 233/234 12/18/92 0-2 in Sandy Gravel 1627 3.25 pCv/g 0.68 Uranium 235 12/18/92 0-2 in Sandy Gravel 1627 3.25 pCv/g 0.68 Uranium 236 12/18/92 0-2 in Sandy Gravel 1627 3.25 pCv/g 0.74 Uranium 238 12/21/92 0-6 ft Sandy Gravel 1627 3.25 pCv/g 0.6913 Uranium 238 12/21/92 0-6 ft Sandy Gravel 1627 3.25 pCv/g 0.6913 Uranium 238 12/21/92 6-12 ft Sandy Gravel 1627 3.25 pCv/g 0.691 Uranium 238 12/21/92 6-12 ft Sandy Gravel 1627 2.42 (lover) pCv/g 0.691 Uranium 238 12/21/92 6-12 ft Sandy Gravel 1627 2.42 (lover) 0.601 0.601 Uranium 238 3/31/83 24-29 4ft Claystone 5.66 173 pCv/g 0.601 Uranium 238 3/31/83						Industrial Use	Flow System					
Uranium 236 12/1892 0-2 in Darky Gravel 1627 3.25 pC/lg 0.69 Uranium 235 12/1892 0-2 in Darky Gravel 113 0.14 pC/lg 0.032 Uranium 236 12/1892 0-6 ft Sandy Gravel 157 3.25 pC/lg 0.043 Uranium 238 12/21/82 0-6 ft Sandy Gravel 113 0.14 pC/lg 0.043 Uranium 238 12/21/82 0-6 ft Sandy Gravel 113 0.14 pC/lg 0.043 Uranium 238 12/21/82 0-6 ft Sandy Gravel 1627 3.25 pC/lg 0.044 Uranium 238 12/21/82 6-12 ft Sandy Gravel 1627 2.42 pC/lg 0.044 Uranium 236 12/21/82 6-12 ft Sandy Gravel 506 173 pC/lg 0.044 Uranium 236 12/21/82 2-12 ft Sandy Gravel 1627 2.42 (lower) pC/lg 0.044 Uranium 238 3/31/83 23 4-29 4 ft Claystone<	SSACOTAAE	1 000					(UTL 99/99)					
Uranium 235 1/2/18/92 0-2 in Sandy Gravel 1/3 0-14 DONG 0.022 Uranium 238 12/18/92 0-2 in Sandy Gravel 150 173 DONG 0.74 Uranium 238 12/21/92 0-6 ft Sandy Gravel 113 0.14 DONG 0.67 Uranium 238 12/21/92 0-6 ft Sandy Gravel 1627 3.25 DONG 0.67 Uranium 238 12/21/92 0-6 ft Sandy Gravel 1627 3.25 DONG 0.67 Uranium 238 12/21/92 6-12 ft Sandy Gravel 1627 2.42 DONG 0.67 Uranium 238 12/21/92 6-12 ft Sandy Gravel 1627 2.42 (lower) 0.64 Uranium 238 33/183 23 4-29.4 ft Claystone 1627 2.42 DONG 0.69 Uranium 238 33/183 24-29.4 ft Claystone 1627 2.42 DONG 1.6 Uranium 238 33/183 34-41 6 ft Claystone <td>100000</td> <td>Oranium 233/234</td> <td>12/18/92</td> <td>5 라</td> <td>Sandy Gravel</td> <td>1627</td> <td>325</td> <td>700</td> <td>000</td> <td></td> <td></td> <td></td>	100000	Oranium 233/234	12/18/92	5 라	Sandy Gravel	1627	325	700	000			
Uranium 238 12/18/92 G-2 in Sandy Gravel 506 173 PCVII 074 Uranium 235 12/21/82 0-6 ft Sandy Gravel 1627 3.25 PCVII 0.041 Uranium 235 12/21/82 0-6 ft Sandy Gravel 113 0.14 PCVII 0.0913 Uranium 236 12/21/82 6-12 ft Sandy Gravel 1627 2.42 (lower) 0.014 Uranium 238 12/21/82 6-12 ft Sandy Gravel 1627 2.42 (lower) 0.0104 Uranium 238 12/21/82 6-12 ft Sandy Gravel 1627 2.42 (lower) PCVII Uranium 238 12/21/82 6-12 ft Sandy Gravel 1627 2.42 (lower) PCVII Uranium 238 3/31/83 23 4-29 4 ft Claystone 1627 2.42 (lower) PCVII Uranium 238 3/31/83 24 4-29 4 ft Claystone 1627 2.42 PCVII 14 Uranium 238 3/31/83 24 4-16 ft Claystone 1627 2.4	5340011AE	Uranium 235	12/18/92	0-2 17	Sandy Gravel	113		300	800	0	023	4
Uranium 233/234 12/21/82 0-6 ft Sandy Gravel 1327 173 PCVIG 074 Uranium 235 12/21/82 0-6 ft Sandy Gravel 1137 0.14 PCVIG 0.691 Uranium 238 12/21/82 0-6 ft Sandy Gravel 150 173 DCVIG 0.491 Uranium 238 12/21/82 6-12 ft Sandy Gravel 150 0.14 PCVIG 0.404 Uranium 238 12/21/82 6-12 ft Sandy Gravel 150 0.14 PCVIG 0.404 Uranium 238 12/21/82 6-12 ft Sandy Gravel 506 173 PCVIG 0.404 Uranium 238/234 3/31/83 23 4-29 4 ft Claystone 150 0.35 PCVIG 1.4 Uranium 238/234 3/31/83 24-29 4 ft Claystone 162 242 PCVIG 1.5 Uranium 238/234 3/31/83 24-36 4 ft Claystone 162 242 PCVIG 1.6 Uranium 238/234 3/31/83 34	SS40011AE	Uranium 238	12/18/92	02 in	Sandy Grave	200	410	BCVG	0 032	0.1	0 064	∢
Uranium 236 12/21/92 0-6 ft Sandy Gravel 102/7 3 25 PC/lg 0 6913 Uranium 238 12/21/92 0-6 ft Sandy Gravel 113 0 14 PC/lg 0 09913 Uranium 238 12/21/92 6-12 ft Sandy Gravel 1627 3.25 PC/lg 0 09913 Uranium 238 12/21/92 6-12 ft Sandy Gravel 1627 3.25 PC/lg 0 0491 Uranium 238 12/21/92 6-12 ft Sandy Gravel 1627 2.42 PC/lg 0 477 Uranium 238/234 3/31/83 23 4-29 4 ft Claystone 1627 2 42 PC/lg 0 467 Uranium 238/234 3/31/83 23 4-29 4 ft Claystone 1627 2 42 PC/lg 0 469 Uranium 238/234 3/31/83 29 4-35 4 ft Claystone 1627 2 42 PC/lg 1 4 Uranium 238/234 3/31/83 28 4-35 4 ft Claystone 1627 2 42 PC/lg 1 6 Uranium 238/234 <td< td=""><td>3H40078AE</td><td>Uranium 233/234</td><td>12/21/92</td><td># 2</td><td>Sandy Glavel</td><td>200</td><td>1/3</td><td>pC/g</td><td>0 74</td><td>0 1</td><td>0.23</td><td>4</td></td<>	3H40078AE	Uranium 233/234	12/21/92	# 2	Sandy Glavel	200	1/3	pC/g	0 74	0 1	0.23	4
Uranium 238 12/21/82 0-6 ft Sandy Gravel 506 173 0 491 0 0913 Uranium 238/234 12/21/82 6-12 ft Sandy Gravel 506 173 0 449 0 491 Uranium 238/234 12/21/82 6-12 ft Sandy Gravel 150 0 14 pCl/g 0 467 Uranium 238/234 3/31/83 23 4-29.4 ft Claystone 1627 2.42 (lower) pCl/g 0 477 Uranium 238/234 3/31/83 23 4-29.4 ft Claystone 1627 2.42 (lower) pCl/g 0 969 Uranium 238/234 3/31/83 29 4-36.4 ft Claystone 1035 pCl/g 0 969 Uranium 238/234 3/31/83 29 4-36.4 ft Claystone 506 1 92 pCl/g 0 044 Uranium 238/234 3/31/83 29 4-36.4 ft Claystone 506 1 92 pCl/g 0 044 Uranium 238/234 3/31/83 36.4-41 6 ft Claystone 506 1 92 pCl/g 0 0/g Uranium 238/234	3H40078AE	Uranium 235	12/21/92	=======================================	Sandy Gravel	35,	325	DC/Q	0 502	0 041	0 176	4
Uranium 238/234 12/21/82 6-12 ft build and build	3H40078AE	Uranium 238	12/01/02	***	Country Critical	21-	0.14	DC/Q	0 0913	0 024	0 0733	4
Uranium 236 1/21/92 6-12 ft Sandy Grave 1627 3.25 pCl/g 0.44 0.404 Uranium 238 1/221/92 6-12 ft Sandy Grave 113 0.14 pCl/g 0.0104 Uranium 238 1/221/92 6-12 ft Sandy Grave 156 1.73 pCl/g 0.0104 Uranium 238 3/31/83 23 4-29 4 ft Claystone 1627 2 42 (lower) pCl/g 0.0104 Uranium 239 3/31/83 29 4-36 4 ft Claystone 506 1 92 pCl/g 1.6 Uranium 239 3/31/83 29 4-36 4 ft Claystone 506 1 92 pCl/g 1.6 Uranium 239 3/31/83 29 4-36 4 ft Claystone 506 1 92 pCl/g 1.6 Uranium 238 3/31/83 36 4-41 6 ft Claystone 1627 2 42 pCl/g 1.0 Uranium 238 3/31/83 36 4-41 6 ft Claystone 1627 2 42 pCl/g 1.0 Uranium 238 3/3	3H40081AE	Uranium 233/234	12/21/02		Sarioy Grave	906	173	pCi/g	0 491	0 024	0 167	
Uranium 238 1221/82 6-1211 Sandy Gravel 113 0 14 pCVg -0.104 Uranium 238 12/21/82 6-1211 Sandy Gravel 506 173 pCVg 0 477 Uranium 235/234 3/31/83 23 4-29.4 ft Claystone 1627 2 42 (lower) pCVg 0 455 Uranium 238 3/31/83 23 4-29.4 ft Claystone 1627 2 42 pCVg 0 059 Uranium 238 3/31/83 29 4-36.4 ft Claystone 1627 2 42 pCVg 1.6 Uranium 239/234 3/31/83 29 4-36.4 ft Claystone 1627 2 42 pCVg 1.6 Uranium 238 3/31/83 36.44.1 ft Claystone 506 1 92 pCVg 1.6 Uranium 235 3/31/83 36.44.1 ft Claystone 506 1 92 pCVg 1.6 Uranium 236 3/31/83 41.6-47.6 ft Silfy Claystone 506 1 92 pCVg 1.7 Uranium 236 3/31/83	3H40081AE	Uranium 235	12/21/02	171-0	Sandy Grave	1627	3.25	pCi/g	9 4 4	0 022	0 143	: 4
Uranium 235/234 127/192 6-12 ft Sandy Gravel 506 173 PCVG 0 477 Uranium 235/234 3/31/83 23 4-29 4 ft Claystone 1627 2 42 (lower) PCVG 0 95 Uranium 235/234 3/31/83 23 4-29 4 ft Claystone 506 1 92 PCVg 1.4 Uranium 236/234 3/31/83 29 4-35 4 ft Claystone 506 1 92 PCVg 1.5 Uranium 238 3/31/83 29 4-35 4 ft Claystone 506 1 92 PCVg 1.5 Uranium 238 3/31/83 36-4-16 ft Claystone 506 1 92 PCVg 1.6 Uranium 238 3/31/83 36-4-16 ft Claystone 506 1 92 PCVg 1.6 Uranium 238 3/31/83 36-4-16 ft Claystone 506 1 92 PCVg 1 9 Uranium 238 3/31/83 416-47 6 ft Sity Claystone 506 1 92 PCVg 1 9 Uranium 238 3/31/83 41	H40081AF	(fraction 238	10,01,00	1171-0	Sandy Grave	113	0 14	D/Od	0.0104	0000	8000	: -
Uranium 235 3/31/83 2/2 4-29.4 ft Claystone 1627 2 42 (lower) PCUIG 0 95 Uranium 235 3/31/83 2/3 4-29.4 ft Claystone 1/3 0 35 PCUIG 0 059 Uranium 238 3/31/83 2/3 4-29.4 ft Claystone 1/3 0 35 PCUIG 1/4 Uranium 238 3/31/83 2/3 4-36.4 ft Claystone 1/3 0 35 PCUIG 1/5 Uranium 238 3/31/83 3/3 4-41.6 ft Claystone 1/6 1/3 PCUIG 1/6 Uranium 239 3/31/83 3/3 4-41.6 ft Claystone 1/6 1/3 PCUIG 1/6 Uranium 239 3/31/83 3/3 4-41.6 ft Claystone 5/6 1/3 PCVIG 1/6 Uranium 238 3/31/83 3/4 6 ft Claystone 5/6 1/3 PCVIG 1/9 Uranium 238 3/31/83 4/1 6 ft Slity Claystone 5/6 1/9 PCVIG 1/7 Uranium 238 3/31/83 4/1	H40429AF	Iraniim 999.994	78/7/20	5-12 II	Sandy Gravel	506	173	Ş	0 477	2000	0.157	<
Uranium 238 3/31/83 22 4-29 4 ft Clay stone 113 0.35 PCVg 0.069 Uranium 233/234 3/31/83 22 4-29 4 ft Clay stone 1627 2 42 PCVg 1.4 Uranium 235/234 3/31/83 29 4-36 4 ft Clay stone 113 0.35 PCVg 1.6 Uranium 235/234 3/31/83 29 4-36 4 ft Clay stone 506 1.92 PCVg 1.6 Uranium 238 3/31/83 36.4-41 6 ft Clay stone 103 DCVg 1.6 Uranium 238 3/31/83 36.4-41 6 ft Clay stone 506 1.92 PCVg 1.9 Uranium 238/234 3/31/83 36.4-41 6 ft Clay stone 506 1.92 PCVg 1.9 Uranium 238/234 3/31/83 41.6-47.6 ft Sity Clay stone 506 1.92 PCVg 1.7 Uranium 238/234 3/31/83 41.6-47.6 ft Sity Clay stone 506 1.92 PCVg 0.1 Uranium 238/234 3/31/83 47.6-60.2 ft Sity Clay stone 1627 2.42 PCVg 0.0 <t< td=""><td>H40429AE</td><td>I frantim 235</td><td>301/83</td><td>23 4-29.4 T</td><td>Claystone</td><td>1627</td><td>2 42 (lower)</td><td>D D D</td><td>960</td><td>0 020</td><td>200</td><td><</td></t<>	H40429AE	I frantim 235	301/83	23 4-29.4 T	Claystone	1627	2 42 (lower)	D D D	960	0 020	200	<
Uranium 239/234 3/31/83 23 4-29 4 ft Cleystone 506 192 pCug 14 Uranium 233/234 3/31/83 29 4-35 4 ft Cleystone 113 0.35 pCug 1.4 Uranium 236 3/31/83 29 4-35 4 ft Cleystone 506 1.92 pCug 1.6 Uranium 236 3/31/83 35.441 6 ft Cleystone 506 1.92 pCug 1.6 Uranium 235 3/31/83 35.441 6 ft Cleystone 506 1.92 pCug 1.6 Uranium 236 3/31/83 35.441 6 ft Cleystone 506 1.92 pCug 1.9 Uranium 238 3/31/83 41.647.6 ft Silty Cleystone 506 1.92 pCug 0.1 Uranium 236 3/31/83 41.647.6 ft Silty Cleystone 506 1.92 pCug 0.1 Uranium 236 3/31/83 47.660.2 ft Silty Cleystone 506 1.92 pCug 0.1 Uranium 238 3/31/83 47.660.	HADAOOAE	200	20100	23 4-29 4 TL	Claystone	113	0 35	Ş	0.059	000	0000	د -
Uranium 235 3/31/83 29 4-36 4 ft Claystone 1627 2 42 pCVg 1.5 Uranium 236 3/31/83 29 4-36 4 ft Claystone 113 0.35 pCVg -0.023 Uranium 238 3/31/83 3.6.4.41 6 ft Claystone 1627 2.42 pCVg 1.6 Uranium 235 3/31/83 3.6.4.41 6 ft Claystone 113 0.35 pCVg 1.6 Uranium 236 3/31/83 3.6.4.1 6 ft Claystone 506 1.92 pCVg 1.7 Uranium 238 3/31/83 4.1.6.47.6 ft Sity Claystone 1627 2.42 pCVg 0.1 Uranium 236 3/31/83 4.1.6.47.6 ft Sity Claystone 1627 2.42 pCVg 0.1 Uranium 238 3/31/83 4.1.6.47.6 ft Sity Claystone 1627 2.42 pCVg 0.1 Uranium 238 3/31/83 4.1.6.47.6 ft Sity Claystone 192 pCVg 0.1 Uranium 238 3/31/83 4.1.6.60.2 ft	HANGEBAE	Uranium 236	3/31/93	23 4-29 4 ft	Claystone	206	192	ζ		0000	2000	∢.
Uranium 235 3/31/83 29 4-36 4 ft Claystone 113 0 35 PCVg -0.023 Uranium 238 3/31/83 36.441 6 ft Claystone 506 1 92 PCVg -0 023 Uranium 235 3/31/83 36.441 6 ft Claystone 113 0 35 PCVg 1 6 Uranium 236 3/31/83 36.41 6 ft Claystone 506 1 92 PCVg 1 9 Uranium 238 3/31/83 41 6 47 6 ft Sity Claystone 1627 2 42 PCVg 1 7 Uranium 239 3/31/83 41 6 47 6 ft Sity Claystone 506 1 92 PCVg 1 7 Uranium 238 3/31/83 41 6 47 6 ft Sity Claystone 506 1 92 PCVg 0.1 Uranium 235 3/31/83 47 6 60.2 ft Sity Claystone 506 1 92 PCVg 0.1 Uranium 238 3/31/83 47 6 60.2 ft Sity Claystone 506 1 92 PCVg 0.1 Uranium 238 3/31/83 <	14000011	Oranium 233/234	3/31/83	29 4-35 4 ft	Claystone	1627	242	900	- 4	200	89	<
Uranium 238 3/31/83 29 4-36 4 ft Claystone 506 1 92 PCVQ -0 023 Uranium 233/234 3/31/83 36.4-16 ft Claystone 1627 2 42 PCVQ 1 6 Uranium 235 3/31/83 36.4-16 ft Claystone 1627 2 42 PCVQ 2.2 Uranium 238 3/31/83 36.4-16 ft Claystone 1627 2 42 PCVQ 1 9 Uranium 238 3/31/83 41.6-47.6 ft Silty Claystone 1627 2 42 PCVQ 1 7 Uranium 238 3/31/83 41.6-47.6 ft Silty Claystone 506 1 92 PCVQ 1 7 Uranium 238 3/31/83 47.6-60.2 ft Silty Claystone 1627 2 42 PCVQ 0.1 Uranium 235 3/31/83 47.6-60.2 ft Silty Claystone 1627 2 42 PCVQ 0.1 Uranium 238 3/31/83 47.6-60.2 ft Silty Claystone 506 1 92 PCVQ 1 16 Uranium 238 3/31/83	H40568AE	Uranium 235	3/31/93	29 4-35 4 ft	Clavetone	140	3000	2	9:1	9800	0 54	⋖
Uranium 239/234 3/31/83 36.441 6 ft Claystone 1627 2 42 pCl/g 16 Uranium 235 3/31/83 36.441 6 ft Claystone 113 0.35 pCv/g 2.2 Uranium 238 3/31/83 36.441 6 ft Claystone 506 1.92 pCv/g 0.044 Uranium 238 3/31/83 41 6 47 6 ft Sity Claystone 1627 2.42 pCv/g 1.9 Uranium 238 3/31/83 41 6 47 6 ft Sity Claystone 506 1.92 pCv/g 0.1 Uranium 239 3/31/83 47 6 60.2 ft Sity Claystone 506 1.92 pCv/g 0.1 Uranium 235 3/31/83 47 6 60.2 ft Sity Claystone 506 1.92 pCv/g 0.054 Uranium 238 3/31/83 47 6 60.2 ft Sity Claystone 506 1.92 pCv/g 0.054 Uranium 238 3/31/83 47 6 60.2 ft Sity Claystone 506 1.92 pCv/g 0.054 Uranium 238 3	H40568AE	Uranium 238	3/31/93	29 4-35 4#	Cleretone	200	650	BCO	0 023	0 11	0 004	4
Uranium 235 3/31/83 36.4416 ft Claystone 113 0.35 PCVG 2.2 Uranium 238 3/31/83 36.4416 ft Claystone 506 1.92 PCVG 0.044 Uranium 238 3/31/83 41.647.6 ft Silty Claystone 1627 2.42 PCVG 1.9 Uranium 236 3/31/83 41.647.6 ft Silty Claystone 506 1.92 PCVG 0.1 Uranium 235 3/31/83 47.6-60.2 ft Silty Claystone 506 1.92 PCVG 0.1 Uranium 235 3/31/83 47.6-60.2 ft Silty Claystone 506 1.92 PCVG 1.6 Uranium 236 3/31/83 47.6-60.2 ft Silty Claystone 506 1.92 PCVG 1.6 Uranium 238 3/31/83 47.6-60.2 ft Silty Claystone 506 1.92 PCVG 1.6 Uranium 238 3/31/83 47.6-60.2 ft Silty Claystone 506 1.92 PCVG 1.6 Uranium 238 3/31/83 <td>H40569AE</td> <td>Uranium 233/234</td> <td>3/31/93</td> <td>36 441 8#</td> <td>Cleristons</td> <td>2007</td> <td>1 92</td> <td>PCivo</td> <td>16</td> <td>0 074</td> <td>0 55</td> <td>4</td>	H40569AE	Uranium 233/234	3/31/93	36 441 8#	Cleristons	2007	1 92	PCivo	16	0 074	0 55	4
Uranium 238 3/31/83 3.6.41 6 ft Claystone 506 1 92 PCVg 0.044 Uranium 235/234 3/31/83 41.6-47.6 ft Sity Claystone 1627 2.42 PCVg 19 Uranium 236 3/31/83 41.6-47.6 ft Sity Claystone 506 1.92 PCVg 17 Uranium 238 3/31/83 47.6-60.2 ft Sity Claystone 506 1.92 PCVg 0.1 Uranium 235 3/31/83 47.6-60.2 ft Sity Claystone 506 1.92 PCVg 1.6 Uranium 238 3/31/83 47.6-60.2 ft Sity Claystone 506 1.92 PCVg 1.6 Uranium 238 3/31/83 47.6-60.2 ft Sity Claystone 506 1.92 PCVg 1.6 Uranium 238 3/31/83 47.6-60.2 ft Sity Claystone 506 1.92 PCVg 1.6	H40569AE	Uranium 235	3/31/83	35.441.8#	Clearatons	36	2 42	PC/g	22	0 0 1 8	0 55	4
Uranium 239/234 3/31/83 41 6-47.6 ft Sity Claystone 1627 2 42 PCVg 17 Uranium 236 3/31/83 41.6-47.6 ft Sity Claystone 113 0.35 PCVg 0.1 Uranium 238 3/31/83 47.6-60.2 ft Sity Claystone 506 1.92 PCVg 0.1 Uranium 235 3/31/83 47.6-60.2 ft Sity Claystone 113 0.35 PCVg 1.6 Uranium 238 3/31/83 47.6-60.2 ft Sity Claystone 506 1.92 PCVg 1.6 Uranium 238 3/31/83 47.6-60.2 ft Sity Claystone 506 1.92 PCVg 1.6 12.1 ft = top of bedrock 12.1 ft = top of bedrock 506 1.92 PCVg 1.6	H40569AE	Uranium 238	3/31/93	35 441 8#	Cleristons	513	035	DC//d	0 0 4 4	0 0 1 8	0 062	V
Uranium 235 3/31/83 41.6-47.6 ft Sity Claystone 113 0.35 pCl/g 17 Uranium 238 3/31/83 41.6-47.6 ft Sity Claystone 506 1.92 pCl/g 0.1 Uranium 235 3/31/83 47.6-60.2 ft Sity Claystone 1627 2.42 pCl/g 1.6 Uranium 236 3/31/83 47.6-60.2 ft Sity Claystone 506 1.92 pCl/g 1.6 Uranium 238 3/31/83 47.6-60.2 ft Sity Claystone 506 1.92 pCl/g 1.6 12.1 ft = top of bedrock 12.1 ft = top of bedrock 506 1.92 pCl/g 1.6	H40570AE	Uranium 233/234	3/31/8/3	41 6.47 8 #	City, Country	985	192	pCi/g	18	0 0 18	0 49	A
Uranium 238 3/31/83 41 6-47 6 ft Silty Cleystone 506 182 PCVg 0.1 Uranium 239/234 3/31/83 47 6-60.2 ft Silty Cleystone 1627 2.42 PCVg 1.6 Uranium 236 3/31/83 47 6-60.2 ft Silty Cleystone 113 0.35 PCVg 1.6 Uranium 238 3/31/83 47 6-60.2 ft Silty Cleystone 506 192 PCVg 1.6 12.1 ft = top of bedrock 12.1 ft = top of bedrock 16 16 16	H40570AE	Uranium 235	3/31/93		Sift Clarific	<u></u>	242	D S S	17	2000	0.25	4
Uranium 235 3/31/83 47 6-60.2 ft Sitty Claystone 506 1 82 pCl/g 7 8 Uranium 235 3/31/83 47 6-60.2 ft Sitty Claystone 113 0 35 pCl/g 1 6 Uranium 238 3/31/83 47 6-60.2 ft Sitty Claystone 506 1 92 pCl/g 1 6 12.1 ft = top of bedrock 12.1 ft = top of bedrock 16 16 16	H40570AE	Uranium 238	3/31/03	44 6 47 6 64	Olly Claystone	5113	0 35	o/Od	0.1	0 0 18	0.05	4
Uranium 235 3/31/83 47.8-60.2 ft Sity Cleystone 113 0.35 pCl/g 1.6 Uranium 238 3/31/83 47.6-60.2 ft Sity Cleystone 506 192 pCl/g 0.064 12.1 ft = top of bedrock 12.1 ft = top of bedrock 506 192 pCl/g 16	H40089AE	Uranium 233/234	3/21/03		Sinty Claystone	900	192	pCi/g		0018	0.27	
Uranium 238 3/31/83 47 6-60.2 ft Sitty Claystone 506 192 pCl/g 0.054 12.1 ft = top of bedrock 12.1 ft = top of bedrock 16 16	H40089AE	Uranium 235	3/31/03	2 50 C	Siny Caystone	1627	242	bCl/g	10	0 022	020	<
12.1 ft = top of bedrock	H40089AE	Iraniim 238	20100	.0-00.4 II	Siny Claystone	113	0 35	\$\overline{\chi_0}{\overline{\chi_0}}	0.054	2000	7000	<
Wp of bedrock		202	001/00	12.00-0	Siffy Claystone	906	1 92	ğ	100	0000	500	<
			12.11		OCK					†	3	<

LOCATION C. ABEGG	C - Accos										
	10000						Method = TRADS	TRADS			
1010	\perp							2			
CUSI_SAMP_	ANALYTE_NAME	COLLECTION	SAMPLE	LITHOLOGY	TIFRI	IDDED	TIMIT CODE	- :: 1020	_		
S S S		_DATE	INTERVAL		Attachment 5.	TOI FRANCE	ON LOOPE MESOLI DELECTIO	TESOL!		HC_SIGMA ASWD	ASWD_
					Subsurface Soil.	LIMIT, Upper				-EHHOH	RATING
					Industrial Use	Flow System					
						(UTL 99/99)					
			0-4 in = Asphalt								
SS40141AE	Uranium 234	11/3/93	4-6 in	Claver Grave	1607	100		A 11 2000 8 2 3			
SS40141AE	Uranium 235	11/3/83	4.5	Clayer, Grave		3.23	1	8	0 108527	10.4	∢
SS40141AE	Uranium 238	11/2/02	100	Clayer Graver		0.14		1.689	0 0757182	0 46	4
BH40715AF	lraniim 224	2007	3	Clayey Gravel	206	173	DC/\d	25.47	0 0903118	431	4
	+63 mmm	28/8/1	0.5-2.25 11	Clayey to	1627	3.25			0 116943	237	4
20110				Sandy Grave			***		2	5	•
BH40/15AE	Uranium 235	11/8/93	0.5-2.25 ft	Clayey to	113	0.14	7/04				
				Sandy Grave		:			5/577800	81.0	∢
BH40717AE	Uranium 234	11/8/93	2.25-4.25#	Sandy Graye	1607	1		河及水南			
BH40717AE	Uranium 235	11/8/93	2 2K.4 2K #	Sendy Crave	36	3.25	D O	1472	0 073596	0 358	V
BH40717AE	Uranium 238	11/8/03	2 25 4 25 4	Court Crave	212	0.14	D O	0 04003	0 0635343	0 0507	4
BH40718AE	Uranium 234	11/0/03	10000	Service Grave	88	173	PC//g	0.938	0 0672922	0.268	4
BH40718AE	Uranium 235	11/0/03	10004	Sandy Graver	1627	3.25	pC//q	2.57	0 0921741	0 583	4
BH40726AE	Uranium 234	11/0/03	10000	Demoy Grave	113	0 14	DC/d	CTEON		0 112	4
BH40726AE	Uranium 235	11/0/02	20101	Caryerone	1627	2 42 (lower)	DCl/g		0 0738923	0 759	4
BH40728AE	Uranium 238	11/9/83	00-701	Claystone	113	0.35	DCiva	0 1164	0 0687081	6060 0	4
BH40728AF	Iraniim 234	44,000	20000	CHRYSTONE	8	192	pCi/g		0 0782628	0.466	4
BH40728AF	I Iraniim 235	110/03	0.0-14.0 1	Claystone	1627	242	pCi/g	1.547	0 0923176	0.418	4
BH40728AE	Iranium 238	11/9/95	0.0-14.8 II	Claystone	113	035		0 03641	0 0696508	0054	4
	200		0.0-14.0 1	Claystone	206	192	DCj/u	1 50	0 07770 400	100	
		6.9 ft =	t = top of bedrock	ock					001/5400	0 463	4
								-	_	-	-

LOCATION_C = 46793	C = 46793						Method = TRADS	TRADS			
CUST_SAMP	ANALYTE_NAME	COLLECTION	SAMPLE	ПТНОСОВУ	TIER 1,	UPPER TOI FRANCE	UNIT_CODE RESULT DETECTION	RESULT	DETECTION	RC_SIGMA ASWD	ASWD_
					Subsurface Soil,	LIMIT, Upper					}
					Industrial Use	Flow System (UTL 99/99)					
			0-3 in = Asphal	*							
SS40142AE	Uranium 234	11/3/93	4-6 in	Surficial Soil	1627	3.25	D/Qd	90.1	0 074923	2	4
SS40142AE	Uranium 235	11/3/93	4-6 in	Surficial Soil	113	0 14	S/Qd	1000	0 074923	0 178	<
SS40142AE	Uranium 238	11/3/93	4-6 in	Surficial Soil	206	173		900	0 085342	1 12	4
BH40729AE	Uranium 234	11/10/93	0 5-2.5 ft	Sandy Gravel	1627	3.25	ğ		0 114282	116	4
BH40729AE	Uranium 235	11/10/93	0 5-2.5 ft	Sandy Gravel	113	0 14			0 103045	0 194	4
BH40729AE	Uranium 238	11/10/93	0 5-2.5 ft	Sandy Gravel	206	173	g/Qd	3	0 142369	0 7 1 9	<
BH40731AE	Uranıum 234	11/10/93	2.5-4 5 ft	Gravelly Clay	1627	3.25	gyod	151	0 137706	041	4
BH40731AE	Uranium 235	11/10/93	2.5-4 5 ft	Gravelly Clay	113	0 14	p/iQd	0 07489	0 118879	0 0952	<
BH40731AE	Uranium 238	11/10/93	2.5-4 5 ft	Gravelly Clay	506	173	pCi/g	0.9931	0 132105	0 374	4
BH40732AE	Uranium 234	11/10/93	4.5-6.5 ft	Clay	1627	3.25	Ş	1 433	0 0904282	0 38	<
BH40732AE	Uranium 235	11/10/93	45-6.5 #	Clay	113	0 14	ß/Od	0 02886	0 0797018	0 0491	<
BH40732AE	Uranium 238	11/10/93	4.5-6.5 ft	Clay	208	173	B/Od	1.233	0 0752509	0 344	<
BH40742AE	Uranium 234	11/10/93	8.5-14.7 ft	Claystone	1627	2 42 (lower)	D/Od	1 445	0 111501	0 458	4
BH40742AE	Uranium 235	11/10/93	8 5-14 7 ft	Claystone	113	0 35	pC/Q	0 09773	0 103679	0 103	<
BH40742AE	Uranium 238	11/10/93	8.5-14.7 ft	Claystone	506	1 92	pCi/g	1.546	0 111501	0 479	<
BH40823AE	Uranium 234	11/10/93	8.5-14.7 ft	Claystone	1627	2 42	pC//g	0 937	0 0897035	0315	4
BH40823AE	Uranium 235	11/10/93	8.5-14 7 #	Claystone	113	0 35	pCi/g	0 06324	0 0996835	0 0718	4
BH40823AE	Uranium 238	11/10/93	8.5-14.7 ft	Claystone	206	1 92	5/JOd	1 123	0 08341	0 352	<
			6.5 ft = top of bedrock	edrock							

57

LOCATION_C = 46893	C = 46893						METHOD * TRADS	TRADS			
CUST_SAMP_	ANALYTE_NAME	COLLECTION	SAMPLE	LITHOLOGY	TIER I,	UPPER	UNIT_CODE RESULT	RESULT	DETECTIO	RC_SIGMA	ASWD
SON SON		_DATE	INTERVAL		Attachment 5,	TOLERANCE			N_LIMIT	ERROR	RATING
					Subsurface Soil,	LIMIT, Upper					
				i		(UTL 99/89)					
		3	0-4 in = Asphall								
SS40143AE	Uranium 234	11/18/93	3 6-6 in	Surficial Soil	1627	325	D/Od	1,009	0 0702298	0 286	4
SS40143AE	Uranium 235	11/18/93	3.6-6 in	Surficial Soil	113	0 14	5/Od	0 03572	0 0823552	0 0531	4
SS40143AE	Uranium 238	11/18/93	3.6-6 In	Surficial Soil	206	1 73	5/jOd	1.118	0 0616558	0 305	4
BH40743AE	Uranium 234	11/19/93	0 5-2.5 ft	Sandy Gravel	1627	3.25	b/j/d	1.026	0 0867504	0312	4
BH40743AE	Uranium 235	11/19/93	0.5-2.5 #	Sandy Gravel		0 14	bC/\d	0.03136	0 0780652	0 0 0 0 0	4
BH40743AE	Uranium 238	11/19/93	0 5-2.5 ft	Sandy Gravel	206	173	b/jOd	0 9262	0 0654505	0.292	4
BH40745AE	Uranium 234	11/19/93	2.5-4.6 ft	Sandy Gravel	1627	3.25	D D/Od	0.8734	0 101194	0 293	4
BH40745AE	Uranium 235	11/19/93	2.5-4.6 ft	Sandy Gravel	113	0.14	D.	0 03844	0 0520139	0 0547	4
BH40745AE	Uranium 238	11/19/93	2.5-4.6 ft	Sandy Gravel		173	bC/Qd	0 7835	0 0842098	0.274	4
BH40746AE	Uranium 234	11/19/93	4.6-6 6 ft	Gravelly Sand	1627	3.25	DCi/d	0 8201	0 0863036	0 255	4
BH40746AE	Uranium 235	11/19/93	46-66#	Gravelly Sand	113	0 14	D/Od	0.02832	0 0626999	0 0439	4
BH40746AE	Uranium 238	11/19/93	46-66#	Gravelly Sand	206	1 73	pCi/g	0.78	0 0714191	0.247	4
BH40748AE	Uranium 234	11/19/93	6.6-8 6 ft	Sandy Gravel	1627	3 25	pCi/g	2.082	0 0654128	0 448	4
BH40748AE	Uranium 235	11/19/93	6 6-8.6 ft	Sandy Gravel		0 14	bCI/d	0 1179	0 0787085	0 0864	4
BH40748AE	Uranium 238	11/19/93	6 6-8.6 ft	Sandy Gravel		1 73	pCi/g	1.578	0.05178	0.37	4
BH40825AE	Uranium 234	11/19/93	6.6-8.6 ft	Sandy Gravel	1627	3.25	pCi/g	1 937	0 0763591	0415	4
BH40825AE	Uranium 235	11/19/93	6.6-8.6 ft	Sandy Gravel	113	0 14	pCi/g	0 1049	0 0486584	0 0763	4
BH40825AE	Uranium 238	11/19/93		Sandy Gravel	206	173	pCi/g	1 531	0 0644935	0 353	4
BH40749AE	Uranium 234	11/19/93	8 6-10 6 ft	Sandy Gravel	1627	3.25	pCi/g	192	0 0869732	0 482	∢
BH40749AE	Uranium 235	11/19/93	•	Sandy Gravel	113	0 14	bCi/g	0 1386	0 0782657	0 103	4
BH40754AE	Uranium 234	11/19/93		Claystone	1627	2 42 (lower)	pCi/g	1.048	0 0886738	03	4
BH40754AE	Uranium 235	11/19/93	1	Claystone	113	0 35	pC//g	0 03163	0 0427938	0 045	4
BH40754AE	Uranium 238	11/19/93	11 5-12.5 ft	Claystone	206	1 92	pCi/g	1.072	0 0692826	0 303	4
BH40826AE	Uranium 234	11/19/93			1627		PCAL	-0.0178	0.257568	0 0 1 7 9	4
BH40826AE	Uranium 235	11/19/93			113		PC∕\L	0 02886	0.281697	0 113	4
BH40826AE	Uranium 238	11/19/93			909		PO/L	0 09325	0.257568	0 158	4
			11 5 ft = top of bedrock	bedrock							

LOCATION C = 46993	3 = 46993						METHOD = TRADS	TRADS				
											-	
CUST_SAMP_	ANALYTE_NAME	COLLECTION	SAMPLE	СІТНОСОВУ	TIER I,	UPPER	UNIT_CODE RESULT	RESULT	DETECTIO N LIMIT	HC_SIGMA ERROR	∢ Œ	ASWD_ RATING
E S		2 60	N IEU VAL		Subsurface Soil,	LIMIT, Upper			,			
					Industrial Use	Flow System (UTL 99/99)						
			0-10 in = Asphal	_						•		
SSAO144AF	I frankm 234	11/22/93		Surficial Soil	1627	3.25	pCl/g		0 100228	202		4
SSA014AF	Uranium 235	11/22/93	10-16 in	Surficial Soil	113	0 14	pCVg		0 0854714	0 183		<
SSAD144AF	Uranium 238	11/22/93	10-16 ln	Surficial Soil	905	1 73	pC//g		0 0806984	7.7	-	«
SS40146AE	Uranium 234	11/22/93	10-16 in	Surficial Soil	1627	3.25	pCl/g		0 0658853	1 19		4
SS40146AE	Uranium 235	11/22/93	10-16 in	Surficial Soil	113	0 14	pCi/g		0 0542426	0 114		<
SS40146AE	Uranium 238	11/22/93	10-16 in	Surficial Soil	206	1 73	S S S		0 048812	19		4
BH40757AE	Uranium 234	11/22/93	1.3-3.1 ft	Sifty Sand	1627	3.25	SQ/Q	± 10	0 0724047	217	-	4
BH40757AE	Uranium 235	11/22/83	1.3-3 1 ft	Sifty Sand	113	0 14	pčiva		0 0546271	0 191		<
BH40757AE	Uranium 238	11/22/83	1.3-3.1 ft	Sifty Sand	206	1 73	pCi/g		0 0754742	181	1	4
BH40830AE	Uranium 234	11/22/93	1.3-3.1 ft	Sifty Sand	1627	3 25	D Q		0 067828	8	-	4
BH40830AE	Uranium 235	11/22/83	1.3-3.1 ft	Silty Sand	113	0 14	DC/Q		0 0697824	0 174		4
BH40830AE	Uranium 238	11/22/93	1,3-3 1 #	Sifty Sand	909	173	SQ/Q		0 0597824	172		4
BH40759AE	Uranium 234	11/22/93	3.3-6 ft	Sandy Gravel	1627	3.25	SVQ		0 084057	11		∢
BH40759AE	Uranium 235	11/22/93	33-611	Sandy Gravel	113	0 14	D D		0 0634184	0 112		4
BH40759AE	Uranium 238	11/22/93	3.3-6 ft	Sandy Gravel	506	173	Š		0 0801154	0803		∢.
BH40768AE	Uranium 234	11/22/93	5.5-7 ft	Claystone	1627	2 42 (lower)	DQ/Q		0 0735647	1 76		4
BH40768AE	Uranium 235	11/22/83	5.5-7 ft	Claystone	113	0 35	ğ		0 0822207	0 164		4
BH40768AE	Uranium 238	11/22/93	5 5-7 ft	Claystone	506	1 92	DC/Q		0 0701151	25		4
BH40770AE	Uranium 234	11/22/93	7.2-13 1 ft	Claystone	1627	242	δίζα	113	1	0 343		4
BH40770AE	Uranium 235	11/22/93	7.2-13 1 ft	Claystone	113	0 35	ğ	0 01176	1	0 0389		4
BH40770AE	Uranium 238	11/22/93	7.2-13 1 ft	Claystone	506	1 92	Š	1 15	0 0909715	035		4
		29	5 5 ft = top of bedrock	ock								

. 59

LOCATION_C = 47093	C = 47093						METHOD - TRADS	TRADS			
CUST_SAMP_ NUM	ANALYTE_NAME	COLLECTION _DATE	SAMPLE	ПТОСОВУ	TIER I, Attachment 5, Subsurface Soil, Industrial Use	UPPER TOLERANCE LIMIT, Upper Flow System (UTL 99/99)	UNIT_CODE RESULT DETECTIO	RESULT	DETECTIO N_UMIT	RC_SIGMA _ERROR	ASWD_ RATING
			0-6 in = Asphalt								
SS40145AE	Uranium 234	11/17/93	05-07 in (?)	Surficial Soil	1627	3.25	pC//g	0.7124	0 159855	0 345	∢
SS40145AE	Uranium 235	11/17/93		Surficial Soil	113	0 14	bCi/g	0 06339	0 140339	0 0985	V
SS40145AE	Uranium 238	11/17/93	0.5-0 7 in (?)	Surficial Soil	206	173	bC//d	1 031	0 126539	0 428	4
BH40771AE	Uranium 234	11/17/93	0 7-2.7 ft	Gravelly Sand	1627	3.25	bCi/g	0 6156	0 115748	0271	∢
				to Sandy Gravel							
BH40771AE	Uranium 235	11/17/93	07-2.7#	Gravelly Sand	113	0 14	B/Od	0 01896	0 109284	0 0505	∢
				to Sandy Gravel							
BH40771AE	Uranium 238	11/17/93	07-2.7 ft	Gravelly Sand	206	1 73	₽CI/g	0 9419	0 109284	0 347	¥
				to Sandy Gravel							
BH40773AE	Uranium 234	11/17/93	2.7-4.7 ft	Sandy Gravel	1627	3.25	pCl/g	0.3624	0 123584	0 198	4
BH40773AE	Uranium 235	11/17/93	2.7-4.7 ft	Sandy Gravel	113	0 14	pC//g	0 02347	0 0635223	0 0471	∢
BH40773AE	Uranıum 238	11/17/93	2.7-4.7 ft	Sandy Gravel	206	1 73	pCvg	0 5164	0 0635223	0.236	4
BH40774AE	Uranium 234	11/17/93	4.8-6 8 ft	Gravel	1627	3.25	pCv/g	1515	0 126215	0 405	۷
BH40774AE	Uranium 235	11/17/93	4.8-6.8 ft	Gravel	113	0 14	pCi/g	0 1186	0 0873965	6960 0	4
BH40774AE	Uranium 238	11/17/93	4.8-6.8 ft	Gravei	909	173	pCi/g	1.377	0 0832983	0 378	V
BH40776AE	Uranium 234	11/18/93	11 8 8-8.8	Gravel	1627	3.25	pC/Q	1.416	0 0707784	0 343	∢
BH40776AE	Uranium 235	11/18/93	6 8-8.8 ft	Gravel	113	0 14	bC/Q	0 01897	0 0758893	000	4
BH40776AE	Uranium 238	11/18/93	6.8-8.8 ft	Grave	206	173	pCv/g	1058	0.0568151	0 284	V